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(72) Inventors:
• SHOJI, Hiromasa
Kawasaki City, Kanagawa 211 (JP)
• SAKASHITA, Masao
Kawasaki City, Kanagawa 211 (JP)
• SAKON, Tadashi
Kawasaki City, Kanagawa 211 (JP)
• TADOKORO, Kenichiro
Kawasaki City, Kanagawa 211 (JP)
• KANEDA, Yoshihiro
Kawasaki City, Kanagawa 211 (JP)

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(74) Representative:
VOSSIUS & PARTNER
Siebertstrasse 4
81675 München (DE)

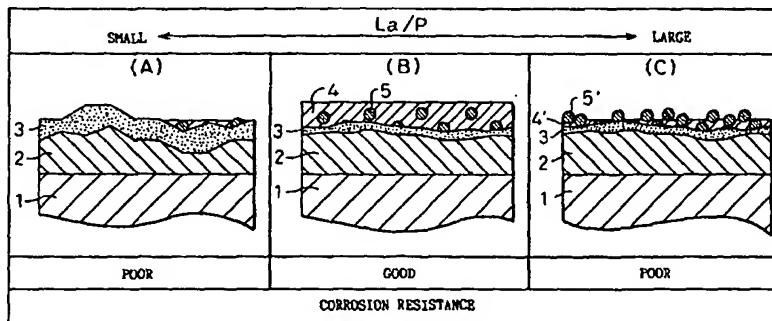
(71) Applicant:
NIPPON STEEL CORPORATION
Tokyo 100-71 (JP)

(54) **SURFACE-TREATED METALLIC MATERIAL WITH CORROSION RESISTANCE AND SURFACE TREATMENT USED THEREFOR**

(57) Surface treated metal materials with corrosion-resistant coating layers composed mainly of oxyacid compounds or rare earth elements (lanthanum, cerium,

etc.), oxyacids or mixtures thereof, and surface treatment agents therefor.

Fig. 1



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Description**Technical Field**

5 [0001] The present invention relates to a surface treated metal material having a coating layer with working-follow-up properties or working conformity and excellent corrosion resistance and containing absolutely no hexavalent chromium, as well as to a surface treatment agent therefor.

Background Art

10 [0002] Coating of chromate films on surfaces as a rust prevention treatment for cold-rolled steel sheets, zinc-plated steel sheets and zinc-based alloy plated steel sheets, aluminum-plated steel sheets, etc. conventionally used for automobiles, household electrical appliances, construction materials and the like, is a common technique. In addition to steel sheets, chromate films are also widely used for petroleum transport pipes and other steel pipes, and for wires and
15 other wiring materials. Aluminum and its alloy surfaces are covered with natural oxides which protect the materials from many types of corrosive environments, but anodic oxidation and chromate treatment are carried out on structural materials for aircraft and the like which require more excellent corrosion resistance and coating adhesion.
[0003] Chromate treatment often used for such metal materials includes electrolytic chromate and application-type chromate. Electrolytic chromate treatment has been carried out by cathodic electrolytic treatment of metal sheets using
20 baths containing, for example, chromic acid as the main component, in addition to sulfuric acid, phosphoric acid, boric acid, halogens and various other anions. Application-type chromate treatment, which has been associated with the problem of elution of chromium from the chromate treated metal sheets, has been carried out by first adding an inorganic colloid or inorganic anion to a solution wherein a portion of the hexavalent chromium has been reduced to trivalent, or a solution with a specified hexavalent chromium and trivalent chromium ratio, to prepare the treatment solution,
25 and then dipping the metal sheet therein or spraying the metal sheet with the treatment solution.

[0004] Among chromate films, those coating layers formed by electrolysis cannot be said to have sufficient corrosion resistance despite the low elution of hexavalent chromium, and their corrosion resistance is particularly low when considerable film damage occurs during working, etc. On the other hand, metal sheets coated with application-type chromate films have high corrosion resistance, and especially excellent worked portion corrosion resistance, but extensive
30 elution of hexavalent chromium from the chromate film becomes a problem. Although elution of hexavalent chromium is controlled considerably by coating with an organic polymer, it is not sufficient. A method generally known as the resin chromate method, such as disclosed in Japanese Unexamined Patent Publication No. 5-230666, gives an improvement in the control of elution of hexavalent chromium, but it is still impossible to avoid elution of trace amounts.

[0005] As a coating method which forms films having the same functions as conventional chromate films but containing absolutely no chromium ions, there is known a method for obtaining a corrosion resistant coating layer of a cerium-containing hydroxide while generating hydrogen gas, by dipping an Al sheet in an acidic aqueous solution of about pH 1 to 3 containing cerium ions, which method is disclosed in Japanese Unexamined Patent Publication (Kohyo) No. 2-502655, a double-salt film of cerium ions, zirconium ions, phosphate ions and fluorine ions on aluminum, which method is disclosed in Japanese Unexamined Patent Publication (Kokai) No. 2-25579, and a zinc phosphate film formed in a
40 zinc ion, phosphate ion and lanthanum compound treatment bath, which method is disclosed in Japanese Unexamined Patent Publication (Kokai) No. 5-331658; however, none of these have adequate working follow-up properties and sufficient corrosion resistance.

[0006] It is an object of the present invention to provide a novel technique for surface treated metal materials having corrosion-resistant coating layers with working follow-up properties and excellent corrosion resistance and employing
45 absolutely no hexavalent chromium.

Disclosure of the Invention

[0007] As a result of much diligent research aimed at designing general use films which have been subjected to conversion treatment instead of the existing chromate treatment, in systems containing absolutely no hexavalent chromium, the present inventors have successfully obtained novel and revolutionary inorganic-based chemically treated films which exhibit the unique functions of the individual components, by converting a rare earth element to an oxyacid compound in the form of a paste to give the working-follow-up properties or working conformity, to thus suppress corrosion by its barrier, inhibit cathodic reaction by the rare earth element ions, and induce oxyacid salt film-type passivation and oxide film-type passivation by creating an excess of the oxyacid, to inhibit anodic reaction.
55 [0008] The elements of the gist of the present invention are as follows.

(1) A surface treated metal material characterized by having a corrosion resistant coating layer composed mainly

of an oxyacid compound or hydrogen oxyacid compound of a rare earth element, or a mixture thereof, on the surface of a metal material.

(2) A surface treated metal material according to (1) above, wherein the rare earth element is yttrium, lanthanum and/or cerium.

5 (3) A surface treated metal material according to (1) or (2) above, wherein the anion species of the oxyacid compound and the hydrogen oxyacid compound is a polyvalent oxyacid anion.

(4) A surface treated metal material according to (3) above, wherein the anion species is phosphate ion, tungstate ion, molybdate ion and/or vanadate ion.

10 (5) A surface treated metal material according to (1) above, wherein the corrosion resistant coating layer is composed mainly of a phosphate compound or hydrogen phosphate compound of yttrium, lanthanum and/or cerium, or a mixture thereof.

(6) A surface treated metal material according to (5) above, wherein the phosphate compound and the hydrogen phosphate compound is an ortho-(hydrogen)phosphate compound, meta-phosphate compound or poly-(hydrogen)phosphate compound, or a mixture thereof.

15 (7) A surface treated metal material according to any of (1) to (6) above, wherein the corrosion resistant coating layer further contains as an added component one or more compounds selected from among oxides, hydroxides, halides and organic acid compounds of rare earth elements.

(8) A surface treated metal material according to (7) above, wherein the rare earth element of the added component is cerium.

20 (9) A surface treated metal material according to (8) above, wherein the rare earth element of the added component is tetravalent cerium.

(10) A surface treated metal material according to any of (1) to (9) above, wherein the corrosion resistant coating further contains as an added component an organic-based corrosion inhibitor.

25 (11) A surface treated metal material according to (10) above, wherein the organic-based corrosion inhibitor is one or more compounds selected from the group consisting of formylated derivatives of N-phenyl-dimethylpyrrole, thioglycolic acid esters represented by $\text{HS}-\text{CH}_2\text{COOC}_n\text{CH}_{2n+1}$ (n is an integer of 1-25) and their derivatives, α -mercapto carboxylic acids represented by $\text{C}_n\text{H}_{2n}(\text{SH})\text{COOH}$ (n is an integer of 1-25) and their derivatives, quinoline and its derivatives, triazinedithiol and its derivatives, gallic acid esters and their derivatives, nicotinic acid and its derivatives, catechol and its derivatives and/or conductive polymers.

30 (12) A surface treated metal material according to any of (1) to (11) above, wherein the corrosion resistant coating layer further contains one or more compounds selected from the group consisting of SiO_2 , Cr_2O_3 , $\text{Cr}(\text{OH})_3$, Al_2O_3 , calcium hydroxide, calcium carbonate, calcium oxide, zinc phosphate, zinc hydrogen phosphate, potassium phosphate, potassium hydrogen phosphate, calcium phosphate, calcium hydrogen phosphate, calcium silicate, zirconium silicate, aluminum phosphate, aluminum hydrogen phosphate, titanium oxide, zirconium phosphate, zirconium hydrogen phosphate, sulfuric acid, sodium sulfate, sodium hydrogen sulfate, phosphoric acid, sodium phosphate and sodium hydrogen phosphate.

35 (13) A surface treatment agent for forming corrosion resistant coating layers on the surfaces of metal materials, characterized by being composed mainly of an oxyacid compound or hydrogen oxyacid compound of a rare earth element, or a mixture thereof.

40 (14) A surface treatment agent according to (13) above, wherein the rare earth element is yttrium, lanthanum and/or cerium.

(15) A surface treatment agent according to (13) or (14) above, wherein the anion species of the oxyacid compound and the hydrogen oxyacid compound is a polyvalent oxyacid anion.

45 (16) A surface treatment agent according to (15) above, wherein the anion species is phosphate ion, tungstate ion, molybdate ion and/or vanadate ion.

(17) A surface treatment agent according to (13) above, wherein the corrosion resistant coating layer is composed mainly of a phosphate compound or hydrogen phosphate compound of yttrium, lanthanum and/or cerium, or a mixture thereof.

50 (18) A surface treatment agent according to (17) above, wherein the phosphate compound and the hydrogen phosphate compound is an ortho-(hydrogen)phosphate compound, meta-phosphate compound or poly-(hydrogen)phosphate compound, or a mixture thereof.

(19) A surface treatment agent according to any of (13) to (18) above, wherein the corrosion resistant coating layer further contains as an added component one or more compounds selected from among oxides, hydroxides, halides and organic oxyacid compounds of rare earth elements.

55 (20) A surface treatment agent according to (19) above, wherein the rare earth element of the added component is cerium.

(21) A surface treatment agent according to (20) above, wherein the rare earth element of the added component is tetravalent cerium.

- (22) A surface treatment agent according to any of (13) to (21) above, wherein the corrosion resistant coating further contains as an added component an organic-based corrosion inhibitor.
- (23) A surface treatment agent according to (22) above, wherein the organic-based corrosion inhibitor is one or more compounds selected from the group consisting of formylated derivatives of N-phenyl-dimethylpyrrole, thioglycolic acid esters represented by $\text{HS}-\text{CH}_2\text{COOC}_n\text{CH}_{2n+1}$ (n is an integer of 1-25) and their derivatives, α -mercapto-carboxylic acids represented by $\text{C}_n\text{H}_{2n}(\text{SH})\text{COOH}$ (n is an integer of 1-25) and their derivatives, quinoline and its derivatives, triazinedithiol and its derivatives, gallic acid esters and their derivatives, nicotinic acid and its derivatives, catechol and its derivatives and/or conductive polymers.
- (24) A surface treatment agent according to any of (13) to (23) above, wherein the corrosion resistant coating layer further contains one or more compounds selected from the group consisting of SiO_2 , Cr_2O_3 , $\text{Cr}(\text{OH})_3$, Al_2O_3 , calcium hydroxide, calcium carbonate, calcium oxide, zinc phosphate, zinc hydrogen phosphate, calcium silicate, zirconium silicate, aluminum phosphate, aluminum hydrogen phosphate, titanium oxide, zirconium phosphate, zirconium hydrogen phosphate, sulfuric acid, sodium sulfate, sodium hydrogen sulfate, phosphoric acid, sodium phosphate and sodium hydrogen phosphate.
- (25) A surface treatment agent which contains 0.05-4 mol/kg of a rare earth compound in terms of the rare earth element, and 0.5-100 moles of a phosphate compound and/or hydrogen phosphate compound in terms of H_3PO_4 to one mole of the rare earth element.
- (26) A surface treatment agent according to (25) above, wherein the rare earth element compound is a phosphate compound, hydrogen phosphate compound, oxide or hydroxide of lanthanum or cerium, or a mixture thereof.
- (27) A surface treatment agent according to (25) or (26) above, wherein the phosphate is an ortho-phosphate, meta-phosphate or poly-phosphate, or a mixture thereof.
- (28) A surface treatment agent according to any of (25) to (27) above, which contains water or a mixture of water and a water-soluble organic solvent as a diluting agent.
- (29) A surface treatment agent according to any of (25) to (28) above, wherein the rare earth element compound is a lanthanum compound, and which further contains a cerium compound in a molar ratio of 1.0-0.001 in terms of cerium to lanthanum and/or an organic-based corrosion inhibitor in a molar ratio of 2-0.001 to lanthanum.
- (30) A surface treatment agent according to any of (25) to (28) above, wherein the rare earth element compound is a cerium compound, and which further contains a lanthanum compound in a molar ratio of 1.0-0.001 in terms of lanthanum to cerium and/or an organic-based corrosion inhibitor in a molar ratio of 2-0.001 to lanthanum.

30 Brief Description of the Drawings

[0009]

Fig. 1 is a schematic drawing showing the relationship between the lanthanum/phosphoric acid mixing ratio and the structure of the corrosion resistant coating.
 Figs. 2 and 3 are graphs showing anode current/potential curves for zinc metal in 0.1 mol/liter NaCl solutions adjusted to pH 8.4.

40 Best Mode for Carrying Out the Invention

- [0010] The present invention will now be explained in more detail.
- [0011] The film of the invention is designed to contain rare earth elements as oxyacid compounds (including hydrogen oxyacid compounds, same hereunder) to form a paste for sufficient working follow-up properties (i.e., conformity when the substrate is worked), in order to suppress corrosion by its barrier effect, inhibit cathodic reaction due to the rare earth element ions, and induce oxyacid salt film-type passivation and oxide film-type passivation by creating an excess of the phosphoric acid, to inhibit anodic reaction. For stronger suppression of the cathodic reaction, another rare earth element compound, especially a cerium compound, may also be added.
- [0012] Oxyacid compounds of rare earth elements include compounds of rare earth elements with oxyacid anions such as phosphate anion, tungstate anion, molybdate anion and vanadate anion, and hydrogen oxyacid compounds include those compounds in which hydrogen is present in a part of the cations. Also, the rare earth elements are the 17 elements Sc, Y, La, Ce, Pr, Nd, Pm, Sm, Eu, Gd, Tb, Dg, Ho, Er, Tm, Yb and Lu.
- [0013] For example, LaPO_4 is the lanthanum phosphate compound, and the corresponding lanthanum hydrogen phosphate compounds are $\text{La}(\text{H}_2\text{PO}_4)_3$ and $\text{La}_2(\text{HPO}_4)_3$.
- [0014] The oxyacid compound and/or hydrogen oxyacid compound of the rare earth element, which is the main component of the corrosion resistant coating of the invention, is theoretically not restricted, but since in paste form amorphous (non-crystalline) inorganic polymers are probably formed, it is believed that a working follow-up property will be exhibited even when the film is formed to greater than a prescribed thickness. Such inorganic coating layers which have

working follow-up properties can be used as anti-corrosion barriers. Even though inorganic polymers are formed, the same effect is obtained even if crystalline or amorphous particles are dispersed and present therein.

[0015] Fig. 1 shows a schematic view of preferred embodiments of coating layers obtained by coating lanthanum/phosphate mixtures on zinc-plated 2 steel sheets 1 with different mixing ratios (La/P). When La/P is small, a crystalline, hard coating 3 is formed substantially like a zinc phosphate coating, and although the working follow-up property is low (Fig. 1/A), a high La/P ratio gives a matrix 4 coating composed mainly of $\text{La}(\text{H}_2\text{PO}_4)_3$ and $\text{La}_2(\text{HPO}_4)_3$ (Fig. 1/B) which is an inorganic polymer and has working follow-up properties (i.e., working conformity). However, even if the La/P ratio is too high, many crystalline LaPO_4 particles 5' are deposited, reducing the matrix portion 4' and lowering the film formability and working follow-up property (Fig. 1/C).

[0016] However, Fig. 1 shows only a schematic of a case according to one method (production method), and the relationship between the specific mixing ratios and coating properties is not universal, being dependent on the type of rare earth element compound and (hydrogen) oxyacid compound and their production method.

[0017] The molar ratio of the rare earth element ion and the oxyacid ion (in terms of the oxyacid ion in the case of a hydrogen oxyacid compound or a mixture containing one) in the film of an oxyacid compound or hydrogen oxyacid compound of a rare earth element, or a mixture thereof (oxyacid ion/rare earth element ion), is generally 0.5-100, preferably 2-50 and more preferably 5-10. At less than 0.5, the working follow-up property is inadequate, and at greater than 100 the film formability is reduced. The source of the rare earth element is not particularly restricted, and rare earth element compounds such as oxides, acetates, carbonates, chlorides and fluorides may be mentioned, with oxides being preferred.

[0018] Also, the working follow-up property and corrosion resistance are not especially affected even if other rare earth element compounds are included as impurities, such as in misch metal and its precursors. A precursor here refers to a substance which is present from a monazite (phosphate) used as the starting material for lanthanum or cerium until a compound is obtained during smelting and purification thereof. The amount of the rare earth element present in the film may be 1 mg/m^2 or greater. At less than 1 mg/m^2 the corrosion resistance is inadequate. Even at greater than 10 g/m^2 there is no notable improvement in the corrosion resistance, and therefore 10 g/m^2 is sufficient from an economical standpoint. On the other hand, the film thickness is preferably at least $0.01 \mu\text{m}$, and more preferably at least $0.1 \mu\text{m}$. At less than $0.01 \mu\text{m}$ the corrosion resistance will be inadequate. However, since there is little improvement in the corrosion resistance even if the film thickness exceeds $5 \mu\text{m}$, it is sufficient at $5 \mu\text{m}$ from an economical standpoint.

[0019] Particularly preferred oxyacid compounds are phosphate compounds and/or hydrogen phosphate compounds, with ortho-phosphate, meta-phosphate or poly-phosphate as the phosphate species. Poly-phosphate based hydrogen phosphate compounds are also suitable.

[0020] One or a mixture of two or more compounds may be used as rare earth elements, with lanthanum, cerium and yttrium, especially lanthanum, being preferred. Cerium is effective for inhibiting cathodic reaction. For example, phosphate compounds and hydrogen phosphate compounds of lanthanum, which are the most preferred compounds, can be easily obtained by chemical reaction between lanthanum compounds including water-soluble inorganic salts such as lanthanum chloride and lanthanum nitrate or oxides such as lanthanum oxide or lanthanum hydroxide, and orthophosphoric acid, poly-phosphoric acid or phosphate salts such as sodium hydrogen phosphate. Here, it is preferred for the starting material to be a lanthanum compound of a water-soluble and volatile acid such as a chloride or nitrate, to facilitate heat removal of the anions other than the phosphate ion, but lanthanum compounds comprising anti-corrosive anions which are insoluble in water and non-volatile, such as molybdate salts and tungstate salts, may also be reacted with phosphoric acid.

[0021] More preferably, a lanthanum phosphate compound or hydrogen phosphate compound is obtained by reaction between an oxide or hydroxide and phosphoric acid. Alternatively, a surface layer obtained by reaction of particles of lanthanum oxide or lanthanum hydroxide with phosphoric acid under relatively mild conditions may be used alone as the phosphate compound mixture. Here, when the lanthanum compound and phosphoric acid coexist, the lanthanum phosphate LaPO_4 may exist alone as a stable phosphate compound, but since oxides and hydroxides of lanthanum cannot exist alone, particle surfaces of oxides and hydroxides must be in admixture with phosphate compounds or hydrogen phosphate compounds. They may also be natural phosphate compounds produced as minerals.

[0022] The corrosion resistant coating layer of the invention may also contain, as added components, oxides, hydroxides, halides, carbonates, sulfates, nitrates and organic acid compounds of rare earth elements, particularly cerium. These compounds, especially tetravalent cerium ions and cerium compounds, are said to have an effect of reinforcing the inhibiting effect on the cathodic reaction. The amount of such an added component is no more than 50-fold, preferably no more than 10-fold, and more preferably no more than 5-fold, in terms of the molar ratio of the added rare earth element with respect to the number of moles of the rare earth element of the oxyacid compound and/or hydrogen oxyacid compound. If the amount of the added component is too great, the film formability is lowered and a film with sufficient working follow-up properties cannot be obtained. Even when the cerium compound is an oxyacid compound or hydrogen oxyacid compound, its addition to the matrix of an oxyacid compound or hydrogen oxyacid compound of the other rare earth element has the effect of reinforcing the cathodic reaction-inhibiting effect, and therefore it may be

added in a molar ratio of 50-fold or less with respect to the other rare earth element.

[0023] The organic-based corrosion inhibitor adheres to the metal surface, and forms a complex during elution of the metal ion and trapping it, thus having the effect of inhibiting further progress of ionization. Organic-based corrosion inhibitors which may be used include compounds possessing, in the molecular structure a functional group (=O, -NH₂,

=NH, =N-, =S, -OH, etc.) required to form metal complex bonds, and a functional group (-OH, =NH, -SH, -CHO, -COOH, etc.) which can form a covalent bond with the metal surface. Incidentally, the organic-based corrosion inhibitor included in the film is preferably a compound which is poorly water-soluble. The reason is that the corrosion inhibiting effect is exhibited when the organic-based corrosion inhibitor dissolves in trace amounts by water passing through the film, and therefore if it is highly water soluble it will easily elute out when water passes through the film, causing the effect to not be exhibited, or resulting in inadequate duration of the effect.

[0024] Specific examples of poorly water-soluble organic-based corrosion inhibitors possessing both of the aforementioned functional groups include formylated derivatives of N-phenyl-dimethylpyrrole, thioglycolic acid esters represented by HS-CH₂COOC_nCH_{2n+1} (n is an integer of 1-25) and their derivatives, α -mercaptopcarboxylic acids represented by C_nH_{2n}(SH)COOH (n is an integer of 1-25) and their derivatives, quinoline and its derivatives, triazine-15 edithiol and its derivatives, gallic acid esters and their derivatives, nicotinic acid and its derivatives, and catechol and its derivatives.

[0025] An electroconductive polymer can also be used as an organic-based corrosion inhibitor with a different anti-corrosion mechanism. This is a molecule of a same repeating unit with π -electron conjugated bonds spread throughout the entire molecule, of which polyacetylene, polyaniline, polythiophene and polypyrrrole are known. By adding a dopant such as barium sulfate, it is possible to confer electric conductivity thereto. The anti-corrosion effects of electroconductive polymers are not understood in detail, but they are assumed to exhibit corrosion resistant current rectification effects and oxygen reduction inhibiting effects at interfaces due to their electroconductivity, and act as cathode corrosion inhibitors.

[0026] These organic-based corrosion inhibitors may be used alone or in mixtures of 2 or more, and the amount thereof added is 0.001-2, preferably 0.01-1 and more preferably 0.02-0.5 in terms of the molar ratio of organic-based corrosion inhibitor to the rare earth element ion (organic-based corrosion inhibitor/rare earth element ion). If the molar ratio is less than 0.001 the effect of addition will be insufficient, and if it is greater than 2 the adhesion will be inadequate.

[0027] Also, the form of these organic-based corrosion inhibitors in the film is not particularly restricted, and they may be included in the film by a method whereby they are added and mixed directly into the treatment solution. Alternatively, they may be predissolved in the phosphate and then added to the treatment solution, or they may be completely dissolved in an alcohol such as ethanol or isopropyl alcohol after which deionizing water is added dropwise to form a fine colloid which is added to the treatment solution.

[0028] In addition to a rare earth element compound such as a cerium compound, etc., an effect of reinforcing the barrier effect of the corrosion resistant coating layer or suppressing elution of the added components can be obtained, or the cathode anticorrosion or anode anticorrosion can be reinforced, by further adding SiO₂, Cr₂O₃, Cr(OH)₃, Al₂O₃, calcium hydroxide, calcium carbonate, calcium oxide, zinc phosphate, zinc hydrogen phosphate, potassium phosphate, potassium hydrogen phosphate, calcium phosphate, calcium hydrogen phosphate, calcium silicate, zirconium silicate, aluminum phosphate, aluminum hydrogen phosphate, titanium oxide, zirconium phosphate, zirconium hydrogen phosphate, sulfuric acid, sodium sulfate, sodium hydrogen sulfate, phosphoric acid, sodium phosphate, sodium hydrogen phosphate, etc.

[0029] The metal material which is the object of the invention is not particularly restricted, and application may be made to surface treated steel sheets and cold-rolled steel sheets, for example fused zinc-plated steel sheets, fused zinc-iron alloy-plated steel sheets, fused zinc-aluminum-magnesium alloy-plated steel sheets, fused aluminum-silicon alloy-plated steel sheets, fused lead-tin alloy-plated steel sheets and other fused plated steel sheets, zinc electroplated steel sheets, zinc-nickel alloy electroplated steel sheets, zinc-iron alloy electroplated steel sheets, zinc-chromium alloy electroplated steel sheets and other electroplated steel sheets, as well as zinc, aluminum and other metal sheets. Further applications include other forms of materials in addition to metal sheets, such as metal wire, metal pipes and the like.

[0030] A typical process for producing a surface treated metal material film according to the invention involves thoroughly mixing the rare earth element compound and the oxyacid, heat treating the mixture (100-200°C, 0.5-24 hours) and adding an organic-based corrosion inhibitor to the resulting paste product if necessary and thoroughly mixing. Added components such as cerium compounds and a sufficient amount of water are also added if necessary. Addition of added components and water can increase the corrosion resistance and film formability. The treatment solution is applied to the metal material, dried and heat treated (for example, at a metal material temperature of 100-200°C for 30 seconds to 1 hour) to obtain the desired surface treated metal material.

[0031] According to one aspect of the present invention there is provided a surface treatment agent which comprises 0.05-4 mol/kg of a rare earth compound in terms of the rare earth element such as lanthanum or cerium, and 0.5-100 moles of a phosphat c mpound and/or hydrogen phosphate compound in terms of H₃PO₄ to one mole of the rar

earth element.

[0032] A rust-preventing coating layer containing no hexavalent chromium and a process for its production are disclosed in International Patent Application Disclosure (Kohyo) WO88/06639, whereby trivalent cerium ion dissolved in a treatment solution is deposited as a hydroxide on the surface of a metal material by cathode reaction, and then hydrogen peroxide is used for oxidation to tetravalency to obtain a CeO₂ layer with an excellent rust prevention property. The coating layer obtained by this process has poor adhesion to metal materials, and it lacks long-lasting corrosion resistance.

[0033] In addition, this CeO₂ film can be expected to have absolutely no working follow-up properties, and this limits its use considerably. Japanese Unexamined Patent Publication (Kokai) No. 5-331658 discloses a surface treatment solution composed mainly of zinc ion, phosphate ion, a lanthanum compound and a film conversion accelerator, and a zinc phosphate treatment process, as a surface treatment process whereby an electrodeposition coating is applied to a metal surface to form a zinc phosphate film with excellent coating adhesion and corrosion resistance; however, the main gist of the disclosure is zinc phosphate treatment by coating, and since the disclosed lanthanum metal concentration contained in the solution is 0.001-3 g/liter, i.e. in terms of the molar concentration, a low value of 7×10^{-6} to 0.22 moles/liter, despite the inclusion of the lanthanum compound in the zinc phosphate treatment film it has not been possible to achieve the high anti-corrosion function with the film alone, as with conventional chromate films.

[0034] The surface treatment agent and treatment bath for aluminum or its alloy disclosed in Japanese Unexamined Patent Publication No. 2-25579 contains cerium ion, zirconium ion, phosphate ion and fluoride ion, and aluminum is etched by the fluoride ion and forms a highly corrosion resistant film with the cerium, zirconium, phosphate and fluoride ion present in the solution; however, the solution composition involves the etching which is limited to the materials of aluminum and its alloys, while the effect is achieved in the low concentration ranges of 10-1000 ppm for cerium ion and 10-500 ppm for phosphate ion.

[0035] Jour. Electrochemical Soc. 1991, Vol.138, p.390 describes inhibition of soft steel anode dissolution by addition of trivalent cerium ion to a corrosion resistant solution, while Corrosion Sci. 1993, Vol.34, p.1774 discloses notable inhibition of reduction of oxygen dissolved in solution using stainless steel which has been subjected to ion implantation with cerium ion under vacuum, although this is not industrially practical. As exemplified by these prior art techniques, cerium is well-known to be effective for improving the corrosion resistance of metal materials, but there is a need for a surface treatment agent which can be applied to metal materials in general and which is suitable for industrial mass production.

[0036] In order to solve this problem, the present inventors have diligently studied surface treatment agents which form corrosion resistant coating layers containing no hexavalent chromium and, as a result, have discovered the surface treatment agent described above, which is composed mainly of a rare earth element such as lanthanum or cerium, and phosphoric acid.

[0037] For convenience in explanation, lanthanum will be referred to as the rare earth element; the surface treatment agent is a surface treatment agent for metal materials which is characterized by being composed mainly of a lanthanum compound and phosphoric acid and a diluting agent, with the lanthanum compound present as a phosphate compound, hydrogen phosphate compound, oxide, hydroxide or a mixture thereof, and by further containing additives such as another rare earth element compound, particularly a cerium compound, and an organic-based corrosion inhibitor. The concentration of the lanthanum compound in the surface treatment agent is the number of moles of lanthanum contained in 1 kg of the surface treatment agent. The number of moles of lanthanum per 1 liter of surface treatment agent is not used because of the high amount of lanthanum compound and phosphoric acid in the treatment agent and the wide range of relative density of the treatment agent, which makes it difficult to express it in terms of volume concentration. The phosphoric acid in the treatment agent refers to phosphate ion and hydrogen phosphate ion which form orthophosphoric acid, meta-phosphoric acid, poly-phosphoric acid and phosphate compounds, and its concentration will be expressed in terms of the molar ratio of H₃PO₄ with respect to lanthanum.

[0038] The phosphate compound or hydrogen phosphate compound of lanthanum which is one of the main components of the treatment agent can be easily obtained by chemical reaction between a lanthanum compound, for example an inorganic salt such as lanthanum chloride or lanthanum nitrate or an oxide such as lanthanum oxide or lanthanum hydroxide, and an ortho-phosphoric acid, poly-phosphoric acid or meta-phosphoric acid or a phosphate salt such as sodium hydrogen phosphate. Here, it is preferred for the starting material to be a lanthanum compound of a volatile acid such as a chloride or nitrate, to facilitate heat removal of the anions, but lanthanum compounds comprising anti-corrosive anions which are non-volatile, such as molybdate salts and tungstate salts, may also be reacted with phosphoric acid. More preferably, a lanthanum phosphate compound or hydrogen phosphate compound is obtained by reaction between an oxide or hydroxide and phosphoric acid. Alternatively, a surface layer alone of the phosphate compound mixture obtained by reaction of particles of lanthanum oxide or lanthanum hydroxide with a phosphoric acid under relatively mild conditions may be used. They may also be natural phosphate compounds produced as minerals.

[0039] The surface treatment agent is composed mainly of a lanthanum compound and phosphoric acid, and more specifically it is composed mainly of a phosphat compound, hydrogen phosphat compound, oxide or hydroxide of lan-

thanum or a mixture thereof and phosphoric acid, in combination with water or a mixture of water and a water-soluble organic solvent as a diluting agent. The organic solvent selected is usually methanol or ethanol for the purpose of reducing the viscosity of the surface treatment agent and increasing the accelerated drying effect. The lanthanum compound used as the starting material for the surface treatment agent may also include many other rare earth element compounds, for example, yttrium, neodymium and cerium, derived from rare earth ores during production and purification and their presence is not a hindrance. The phosphoric acid used is ortho-phosphoric acid, meta-phosphoric acid, polyphosphoric acid or a mixture thereof. Here, polyphosphoric acid with the average molecular formula $H_6P_4O_{13}$ is a tetramer of H_3PO_4 , i.e. 4 moles of H_3PO_4 in one mole of the poly-phosphoric acid.

[0040] The concentration of the lanthanum compound contained in the surface treatment agent is characterized by being 0.05-4 mol/kg in terms of lanthanum. The lower limit of 0.05 mol/kg for the concentration of the lanthanum compound is the minimum concentration required to coat a metal material with a lanthanum compound/phosphoric acid-based film having the same excellent corrosion resistance as a chromate film, and it is more preferably 0.1 mol/kg or greater. The upper concentration limit of 4 mol/kg is the upper limit which can give a relatively hard paste-form treatment agent comprising a lanthanum compound, phosphoric acid and a slight amount of diluting agent, to form a uniform coating layer on a metal material surface, and the lanthanum compound concentration is more preferably no greater than 2 mol/kg.

[0041] Also, the major components of the surface treatment agent are the lanthanum compound and phosphoric acid, and it is characterized by containing 0.5-100 moles of phosphoric acid in terms of H_3PO_4 to one mole of the lanthanum compound in terms of lanthanum. The lower limit for the molar ratio of lanthanum to phosphoric acid is the minimum phosphoric acid necessary to coat a metal material surface with the lanthanum compound. Further lowering of the proportion of phosphoric acid will result in a lack of phosphate ions to contribute to adhesion with the metal material surface, due to consumption of phosphate ions as they react with the particle surfaces of the lanthanum oxide or hydroxide compound, thus producing lower corrosion resistance, and in particular, the working follow-up property of the film will become notably inadequate resulting in lower worked portion corrosion resistance. In order to obtain a film with excellent corrosion resistance, the molar ratio of lanthanum to phosphoric acid should be at least 0.5, and especially for obtaining films with excellent worked portion corrosion resistance, it is preferably at least 2, and more preferably at least 5. Such an excess of phosphoric acid is effective for forming the lanthanum hydrogen phosphate compound, while the metal element in the metal material surface also reacts with zinc, for example, to form a zinc phosphate compound, thus increasing the adhesion of the coating layer and having the effect of improving the corrosion resistance of the coating layer composed mainly of the lanthanum compound and phosphoric acid.

[0042] The surface treatment agent for metal materials according to the invention may also contain another rare earth compound, such as a cerium compound, and an organic-based corrosion inhibitor for a still greater rust-prevention effect of the resulting coating layer. The cerium compound added may be one or more compounds selected from among phosphate, hydrogen phosphate, oxide, hydroxide, halide, carbonate, sulfate, nitrate, organic acid compounds and the like, and the valency of the selected cerium may be 3, 4 or a combination thereof. The amount of the added cerium compound is from a molar ratio of 1 to 0.001 in terms of cerium to lanthanum. If the molar ratio of cerium to lanthanum is high, for example 1-0.1, it becomes a major constituent component of the coating layer together with the lanthanum compound and phosphoric acid, and therefore a cerium compound with low solubility, such as a phosphate, hydrogen phosphate, oxide, hydroxide or mixture thereof, is preferably selected. At a molar ratio of 0.1-0.001, compounds with low solubility, as well as soluble cerium compounds such as the aforementioned halides, may also be preferably selected.

[0043] The organic-based corrosion inhibitor may be one of the compounds mentioned previously.

[0044] The amount of the organic-based corrosion inhibitor to be added is at a molar ratio of 2-0.001 to the lanthanum, and the molar ratio for addition is selected not only for reinforcement of the corrosion inhibiting effect but also depending on the composition of the surface treatment agent and the method of forming the coating layer. For example, in the case of an organic-based corrosion inhibitor which strongly binds to the metal ion which corrodes out of the metal material, such as a combination with a quinoline derivative, an effect can be achieved at a low concentration with a molar ratio to lanthanum of 0.01-0.001.

[0045] In the case of a type of corrosion inhibitor which adheres to the metal material surface to inhibit anodic reaction, such as a formylated derivative of N-phenyldimethylpyrrole, a high proportion at a molar ratio of 0.01 or greater is advantageous if the purpose of addition is especially that of suppressing metal dissolution and generation of hydrogen during the process of forming the coating layer. Also, a molar ratio to lanthanum of 0.1 or greater may be used if the purpose of addition is for the organic-based corrosion inhibitor to also constitute one of the main components of the coating layer, and for example by adding the electroconductive polymer polyaniline, it is possible to confer electroconductivity to the coating layer while also giving it a corrosion resistant function. If the molar ratio is less than 0.001, the effect of adding the organic-based corrosion inhibitor will be inadequate, and at greater than 2 the adhesion with the coating layer will be insufficient and the working follow-up property will be impaired.

[0046] The molar ratio of the organic-based corrosion inhibitor with respect to the lanthanum is also selected based

on the desired thickness of the film layer, and for example when forming a thick coating layer for strongly corrosive environments, a sufficient effect can be achieved since the absolute amount of the organic-based corrosion inhibitor in the coating layer is high even if its molar ratio to lanthanum is low and in the order of 0.01. On the other hand, when using a diluted treatment agent with a low lanthanum concentration for the purpose of forming a thin coating layer for weakly corrosive environments, the organic-based corrosion inhibitor is preferably present at a high molar ratio of 0.1-2 with respect to lanthanum.

[0047] The above explanation has been made with lanthanum selected as the rare earth element, but the same effect of the treatment agent of the invention is achieved even if lanthanum is replaced with another rare earth element such as cerium. When lanthanum is replaced with cerium, a lanthanum compound is preferred as the other rare earth compound used in combination therewith.

[0048] This surface treatment agent is a surface treatment agent for metal materials characterized by being composed mainly of a rare earth element compound and phosphoric acid, with water or a mixture of water and a water-soluble organic solvent as a diluting medium. Diluting mediums include the water included in the starting material used in the process for producing the surface treatment agent, the water or organic solvent used for dissolution of the starting material, and the water or organic solvent for dilution of the original treatment agent. Depending on the relative amount of the diluting agent with respect to the rare earth element compound, the phosphoric acid, the other rare earth element compound and the organic-based corrosion inhibitor, the surface treatment agent will exhibit a hard paste form, a soft paste form, a colloid form or a solution form with low solid dispersion, and the range of the dilution may be determined based on the degree of corrosion resistance desired for the film and the method of coating the metal material surface with the film.

[0049] For example, surface treatment agents with a low molar ratio of phosphoric acid to the rare earth element and a high rare earth element concentration are effective for forming highly corrosion resistant films of 1-10 µm thickness by coating methods. If the degree of dilution is increased by addition of water or a water-soluble organic solvent, surfaces can be coated with films of 0.1-1 µm by spray methods. The degree of dilution may also be increased for coating films of 0.1 µm and less by dipping methods.

[0050] This treatment agent exhibits strong acidity, but the hydrogen ion concentration (pH) may optionally be adjusted depending on the purpose or the type of metal material to be surface treated.

[0051] An added component such as SiO₂ or Al₂O₃ mentioned above may also be dispersed in the treatment agent for the purpose of supplementing the rust-preventing effect of a coating layer which has the rare earth element compound and phosphoric acid as the main components and further contains another rare earth element compound and an organic-based corrosion inhibitor.

[0052] The method for applying the present invention to these metal materials is not particularly restricted, and any conventional publicly known method may be used including dipping, spraying and painting, while the method of drying may be appropriately selected within a temperature range of from room temperature to a high temperature of about 300°C, depending on the performance demanded for the coating layer, the treatment agent composition and the method of forming the coating layer.

Examples

[0053] [Examples 1-6]

(Preparation method for treatment solution)

Example 1

[0053]

[1] After thoroughly mixing 32.6 g of lanthanum oxide with 69.2 g, 115.3 g and 173.0 g of phosphoric acid (85%), the mixtures were heated at 100-200°C for 0.5 to 24 hours, and the resulting paste-like products were used as treatment solutions (Samples No.1 to 3 in Table 1).

To treatment solution No.2 there were added lanthanum hydroxide, cerium oxide, cerium hydroxide, cerium chloride and cerium acetate each with a molar ratio of 1:10 for cerium to lanthanum, and these were mixed to make treatment solutions (No.4 to 8 in Table 1).

[2] In [1] above, the phosphoric acid was replaced with 261.0 g of an aqueous ammonium tungstate solution (4%) as 5(NH₄)₂O · 12WO₃ · 5H₂O, 176.6 g of an ammonium molybdate solution (28%) as (NH₄)₆ · Mo₇O₂₄ · 4H₂O and 117.0 g of an aqueous ammonium vanadate solution (5%), as NH₄ · VO₃ which were added and mixed therewith to give paste-like products (Samples No. 9, 15 and 21 in Table 1), and then lanthanum hydroxide, cerium oxide, cerium hydroxide, cerium chloride and cerium acetate were combined therewith in the same manner as in [1] above.

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(Samples No.10-14, 16-20 and 22-26 in Tables 1 and 2).

Example 2

- 5 [0054] Treatment solutions (Samples No. 27-52 in Table 2) were prepared in the same manner as Example 1, except that 23.5 g of cerium phosphate was used instead of lanthanum oxide.

Example 3

- 10 [0055] Treatment solutions (Samples No. 53-78 in Table 3) were prepared in the same manner as Example 1, except that 30.3 g of yttrium chloride hexahydrate was used instead of lanthanum oxide.

Example 4

- 15 [0056] Treatment solutions (Samples No. 79-104 in Table 4) were prepared in the same manner as Example 1, except that 39.6 g of neodymium chloride hexahydrate was used instead of lanthanum oxide.

[0057] All of the reagents used in Examples 1-4 were commercially available products.

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Table 1

Sample No.	Rare earth element	Oxyacid	Additive			
			lanthanum hydroxide	cerium oxide	cerium hydroxide	cerium chloride
1	lanthanum oxide	32.6 g phosphoric acid	62.9 g	-	-	-
2	lanthanum oxide	32.6 g phosphoric acid	115.3 g	-	-	-
3	lanthanum oxide	32.6 g phosphoric acid	173.0 g	-	-	-
4	lanthanum oxide	32.6 g phosphoric acid	115.3 g	3.8 g	-	-
5	lanthanum oxide	32.6 g phosphoric acid	115.3 g	-	3.4 g	-
6	lanthanum oxide	32.6 g phosphoric acid	115.3 g	-	-	4.2 g
7	lanthanum oxide	32.6 g phosphoric acid	115.3 g	-	-	7.5 g
8	lanthanum oxide	32.6 g phosphoric acid	115.3 g	-	-	6.7 g
9	lanthanum oxide	32.6 g aqueous ammonium tungstate	261.0 g	-	-	-
10	lanthanum oxide	32.6 g aqueous ammonium tungstate	261.0 g	3.8 g	-	-
11	lanthanum oxide	32.6 g aqueous ammonium tungstate	261.0 g	-	3.4 g	-
12	lanthanum oxide	32.6 g aqueous ammonium tungstate	261.0 g	-	-	4.2 g
13	lanthanum oxide	32.6 g aqueous ammonium tungstate	261.0 g	-	-	7.5 g
14	lanthanum oxide	32.6 g aqueous ammonium tungstate	261.0 g	-	-	6.7 g
15	lanthanum oxide	32.6 g aqueous ammonium molybdate	176.6 g	-	-	-
16	lanthanum oxide	32.6 g aqueous ammonium molybdate	176.6 g	3.8 g	-	-
17	lanthanum oxide	32.6 g aqueous ammonium molybdate	176.6 g	-	3.4 g	-
18	lanthanum oxide	32.6 g aqueous ammonium molybdate	176.6 g	-	-	4.2 g
19	lanthanum oxide	32.6 g aqueous ammonium molybdate	176.6 g	-	-	7.5 g
20	lanthanum oxide	32.6 g aqueous ammonium molybdate	176.6 g	-	-	6.7 g
21	lanthanum oxide	32.6 g aqueous ammonium vanadate	117.0 g	-	-	-
22	lanthanum oxide	32.6 g aqueous ammonium vanadate	117.0 g	3.8 g	-	-
23	lanthanum oxide	32.6 g aqueous ammonium vanadate	117.0 g	-	3.4 g	-
24	lanthanum oxide	32.6 g aqueous ammonium vanadate	117.0 g	-	-	4.2 g
25	lanthanum oxide	32.6 g aqueous ammonium vanadate	117.0 g	-	-	7.5 g
26	lanthanum oxide	32.6 g aqueous ammonium vanadate	117.0 g	-	-	6.7 g

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Table 2
Oxyacid

Sample No.	Rare earth element		Additive	Lanthanum			Cerium			Cerium acetate
				hydroxide	cerium oxide	cerium hydroxide	cerium chloride	cerium		
27	cerium phosphate	23.5 g	phosphoric acid	57.7 g	-	-	-	-	-	-
28	cerium phosphate	23.5 g	phosphoric acid	115.3 g	-	-	-	-	-	-
29	cerium phosphate	23.5 g	phosphoric acid	230.6 g	-	-	-	-	-	-
30	cerium phosphate	23.5 g	phosphoric acid	115.3 g	3.8 g	-	-	-	-	-
31	cerium phosphate	23.5 g	phosphoric acid	115.3 g	-	3.4 g	-	-	-	-
32	cerium phosphate	23.5 g	phosphoric acid	115.3 g	-	-	4.2 g	-	-	-
33	cerium phosphate	23.5 g	phosphoric acid	115.3 g	-	-	-	7.5 g	-	-
34	cerium phosphate	23.5 g	phosphoric acid	115.3 g	-	-	-	-	6.7 g	-
35	cerium phosphate	23.5 g	aqueous ammonium tungstate	261.0 g	3.8 g	-	-	-	-	-
36	cerium phosphate	23.5 g	aqueous ammonium tungstate	261.0 g	-	3.4 g	-	-	-	-
37	cerium phosphate	23.5 g	aqueous ammonium tungstate	261.0 g	-	-	4.2 g	-	-	-
38	cerium phosphate	23.5 g	aqueous ammonium tungstate	261.0 g	-	-	-	7.5 g	-	-
39	cerium phosphate	23.5 g	aqueous ammonium tungstate	261.0 g	-	-	-	-	6.7 g	-
40	cerium phosphate	23.5 g	aqueous ammonium tungstate	261.0 g	-	-	-	-	-	-
41	cerium phosphate	23.5 g	aqueous ammonium molybdate	176.6 g	3.8 g	-	-	-	-	-
42	cerium phosphate	23.5 g	aqueous ammonium molybdate	176.6 g	-	3.4 g	-	-	-	-
43	cerium phosphate	23.5 g	aqueous ammonium molybdate	176.6 g	-	-	4.2 g	-	-	-
44	cerium phosphate	23.5 g	aqueous ammonium molybdate	176.6 g	-	-	-	7.5 g	-	-
45	cerium phosphate	23.5 g	aqueous ammonium molybdate	176.6 g	-	-	-	-	6.7 g	-
46	cerium phosphate	23.5 g	aqueous ammonium molybdate	176.6 g	-	-	-	-	-	-
47	cerium phosphate	23.5 g	aqueous ammonium vanadate	117.0 g	3.8 g	-	-	-	-	-
48	cerium phosphate	23.5 g	aqueous ammonium vanadate	117.0 g	-	3.4 g	-	-	-	-
49	cerium phosphate	23.5 g	aqueous ammonium vanadate	117.0 g	-	-	4.2 g	-	-	-
50	cerium phosphate	23.5 g	aqueous ammonium vanadate	117.0 g	-	-	-	7.5 g	-	-
51	cerium phosphate	23.5 g	aqueous ammonium vanadate	117.0 g	-	-	-	-	6.7 g	-
52	cerium phosphate	23.5 g	aqueous ammonium vanadate	117.0 g	-	-	-	-	-	-

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Table 3

Sample No.	Rare earth element	Oxyacid	Additive			
			lanthanum hydroxide	cerium hydroxide	cerium chloride	cerium acetate
53	yttrium chloride·6H ₂ O	30.3 g	phosphoric acid	57.7 g	-	-
54	yttrium chloride·6H ₂ O	30.3 g	phosphoric acid	115.3 g	-	-
55	yttrium chloride·6H ₂ O	30.3 g	phosphoric acid	230.6 g	-	-
56	yttrium chloride·6H ₂ O	30.3 g	phosphoric acid	115.3 g	3.8 g	-
57	yttrium chloride·6H ₂ O	30.3 g	phosphoric acid	115.3 g	-	-
58	yttrium chloride·6H ₂ O	30.3 g	phosphoric acid	115.3 g	3.4 g	-
59	yttrium chloride·6H ₂ O	30.3 g	phosphoric acid	115.3 g	-	-
60	yttrium chloride·6H ₂ O	30.3 g	phosphoric acid	115.3 g	4.2 g	-
61	yttrium chloride·6H ₂ O	30.3 g	aqueous ammonium tungstate	261.0 g	-	-
62	yttrium chloride·6H ₂ O	30.3 g	aqueous ammonium tungstate	261.0 g	3.8 g	-
63	yttrium chloride·6H ₂ O	30.3 g	aqueous ammonium tungstate	261.0 g	-	-
64	yttrium chloride·6H ₂ O	30.3 g	aqueous ammonium tungstate	261.0 g	3.4 g	-
65	yttrium chloride·6H ₂ O	30.3 g	aqueous ammonium tungstate	261.0 g	-	-
66	yttrium chloride·6H ₂ O	30.3 g	aqueous ammonium tungstate	261.0 g	-	-
67	yttrium chloride·6H ₂ O	30.3 g	aqueous ammonium molybdate	176.6 g	-	-
68	yttrium chloride·6H ₂ O	30.3 g	aqueous ammonium molybdate	176.6 g	3.8 g	-
69	yttrium chloride·6H ₂ O	30.3 g	aqueous ammonium molybdate	176.6 g	-	-
70	yttrium chloride·6H ₂ O	30.3 g	aqueous ammonium molybdate	176.6 g	-	-
71	yttrium chloride·6H ₂ O	30.3 g	aqueous ammonium molybdate	176.6 g	-	-
72	yttrium chloride·6H ₂ O	30.3 g	aqueous ammonium molybdate	176.6 g	-	-
73	yttrium chloride·6H ₂ O	30.3 g	aqueous ammonium vanadate	117.0 g	-	-
74	yttrium chloride·6H ₂ O	30.3 g	aqueous ammonium vanadate	117.0 g	3.8 g	-
75	yttrium chloride·6H ₂ O	30.3 g	aqueous ammonium vanadate	117.0 g	-	-
76	yttrium chloride·6H ₂ O	30.3 g	aqueous ammonium vanadate	117.0 g	3.4 g	-
77	yttrium chloride·6H ₂ O	30.3 g	aqueous ammonium vanadate	117.0 g	-	-
78	yttrium chloride·6H ₂ O	30.3 g	aqueous ammonium vanadate	117.0 g	4.2 g	-
				-	7.5 g	-
				-	-	6.7 g

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Table 4

Sample No.	Rare earth element	Oxyacid	Additive			
			lanthanum hydroxide	cerium oxide	cerium hydroxide	cerium chloride acetate
79	neodymium chloride·6H ₂ O	39.6 g phosphoric acid	57.7 g	-	-	-
80	neodymium chloride·6H ₂ O	39.6 g phosphoric acid	115.3 g	-	-	-
81	neodymium chloride·6H ₂ O	39.6 g phosphoric acid	230.6 g	-	-	-
82	neodymium chloride·6H ₂ O	39.6 g phosphoric acid	115.3 g	3.8 g	-	-
83	neodymium chloride·6H ₂ O	39.6 g phosphoric acid	115.3 g	-	3.4 g	-
84	neodymium chloride·6H ₂ O	39.6 g phosphoric acid	115.3 g	-	4.2 g	-
85	neodymium chloride·6H ₂ O	39.6 g phosphoric acid	115.3 g	-	-	7.5 g
86	neodymium chloride·6H ₂ O	39.6 g phosphoric acid	115.3 g	-	-	6.7 g
87	neodymium chloride·6H ₂ O	39.6 g aqueous ammonium tungstate	261.0 g	-	-	-
88	neodymium chloride·6H ₂ O	39.6 g aqueous ammonium tungstate	261.0 g	3.8 g	-	-
89	neodymium chloride·6H ₂ O	39.6 g aqueous ammonium tungstate	261.0 g	-	3.4 g	-
90	neodymium chloride·6H ₂ O	39.6 g aqueous ammonium tungstate	261.0 g	-	-	-
91	neodymium chloride·6H ₂ O	39.6 g aqueous ammonium tungstate	261.0 g	-	4.2 g	-
92	neodymium chloride·6H ₂ O	39.6 g aqueous ammonium tungstate	261.0 g	-	-	7.5 g
93	neodymium chloride·6H ₂ O	39.6 g aqueous ammonium molybdate	176.6 g	-	-	-
94	neodymium chloride·6H ₂ O	39.6 g aqueous ammonium molybdate	176.6 g	3.8 g	-	-
95	neodymium chloride·6H ₂ O	39.6 g aqueous ammonium molybdate	176.6 g	-	3.4 g	-
96	neodymium chloride·6H ₂ O	39.6 g aqueous ammonium molybdate	176.6 g	-	-	-
97	neodymium chloride·6H ₂ O	39.6 g aqueous ammonium molybdate	176.6 g	-	4.2 g	-
98	neodymium chloride·6H ₂ O	39.6 g aqueous ammonium molybdate	176.6 g	-	-	7.5 g
99	neodymium chloride·6H ₂ O	39.6 g aqueous ammonium vanadate	117.0 g	-	-	-
100	neodymium chloride·6H ₂ O	39.6 g aqueous ammonium vanadate	117.0 g	3.8 g	-	-
101	neodymium chloride·6H ₂ O	39.6 g aqueous ammonium vanadate	117.0 g	-	3.4 g	-
102	neodymium chloride·6H ₂ O	39.6 g aqueous ammonium vanadate	117.0 g	-	-	-
103	neodymium chloride·6H ₂ O	39.6 g aqueous ammonium vanadate	117.0 g	-	4.2 g	-
104	neodymium chloride·6H ₂ O	39.6 g aqueous ammonium vanadate	117.0 g	-	-	7.5 g
					-	6.7 g

Example 5

- [0058] After thoroughly mixing 32.6 g of lanthanum oxide and 115.3 g of phosphoric acid (85%) as shown in Table 13, the mixture was heated at 150°C for 12 hours and 1 g of each organic-based corrosion inhibitor was added to the resulting paste-like products to make treatment solutions (No. 151-165 in Table 13).
- [0059] Also, adjuvants were added to treatment solution No. 161 to a molar ratio of 1:10 for cerium to lanthanum, and mixed to make treatment solutions (No. 166-173 in Table 14).
- [0060] In Examples 5 and 6, the α -mercaptoplauric acid and N-phenyl-3-formyl-2,5-dimethylpyrrole were synthesized, and all the other components were commercially available reagents.

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Example 6

- [0061] After thoroughly mixing 23.5 g Of cerium phosphate and 115.3 g of phosphoric acid (85%) as shown in Table 15, the mixture was heated at 150°C for 12 hours. One gram of each organic-based inhibitor was added to the resulting paste-like products to make treatment solutions (No. 174-188 in Table 15).
- [0062] Also, adjuvants were added to treatment solution No. 184 to a molar ratio of 1:10 for the cerium contained therein to the cerium compound, and mixed to make treatment solutions (No.189-195 in Table 16).

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(Film-forming method)

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- [0063] Each treatment solution was applied to a metal sheet to a dry film thickness of 1 μm using a bar coater, and then heat treated at a sheet temperature of 100-200°C for 30 seconds to one hour. The metal sheet used was GI (fused zinc-plated steel sheet, plating coverage: 90 g/m²), EG (zinc-electroplated steel sheet, plating coverage: 20 g/m²) or AL (fused aluminum-silicon alloy-plated steel sheet, plating coverage: 120 g/m², Al/Si = 90/10).
- [0064] Incidentally, as a chromate-treatment solution for comparison with chromate-treated steel sheets, a treatment bath was prepared containing 30 g/l of partially starch-reduced chromic acid in terms of CrO₃, 40 g/l of SiO₂ and 20 g/l of phosphoric acid, and films were formed by application, drying and hardening onto the steel sheets. (The amount of Cr in the films was 100 mg/m² in terms of Cr metal).

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(Evaluation of film performance)

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(a) Working follow-up property test

- [0065] After subjecting the sample to 7 mm Erichsen working, it was observed by SEM to evaluate the working follow-up property.

[0066] Evaluation scale:

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- Ⓐ: no cracking
- : slight cracking
- △: slight peeling
- ✗: large cracking, large area peeling

(b) Flat sheet corrosion resistance test

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- [0067] The corrosion resistance was evaluated based on the rusted area after spraying the sample with 5%, 35°C saline. The spraying period was 10 days for GI and EG and 15 days for AL, and the white rust incidence was measured in all cases. Cold-rolled steel sheets were sprayed with saline for 2 hours and the red rust incidence was measured, while aluminum sheets were dipped for 30 minutes in 100°C boiling water and the black rust incidence was measured.

[0068] Evaluation scale:

50

- Ⓐ: 0% rust incidence
- : less than 5% rust incidence
- △: from 5% to less than 20% rust incidence
- ✗: 20% or greater rust incidence

55

(c) Worked corrosion resistance test

- [0069] After 7 mm Erichsen working of th sample, the worked corrosion resistance was evaluated based on the

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rusted area after spraying with 5%, 35°C salin . The spraying period was 10 days for GI and EG and 15 days for AL, and the white rust incidence was measured for all cases.

[0070] Evaluation scale:

- 5 ◎: 0% rust incidence
- o: less than 5% rust incidence
- Δ: from 5% to less than 20% rust incidence
- x: 20% or greater rust incidence

10 Results

[0071] The results of evaluation for Examples 1-6 are listed in Tables 5-16.

[0072] As shown in these tables, the surface treated metal sheets of the present invention had excellent working follow-up properties and exhibited the same flat sheet and worked part corrosion resistances as chromate-treated sheets.

- 15 Consequently, they exhibit their effect as corrosion resistant films containing absolutely no hexavalent chromium and exhibiting excellent environmental suitability as conversion treatment films.

Table 5

No.	Metal sheet	Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
1	EG	◎	◎	◎
	GI	◎	o	o
	AL	◎	o	o
2	EG	◎	o	o
	GI	◎	o	o
	AL	◎	o	o
3	EG	o	o	o
	GI	o	o	o
	AL	o	o	o
4	EG	◎	◎	◎
	GI	◎	o	o
	AL	◎	◎	◎
5	EG	◎	◎	◎
	GI	o	o	o
	AL	o	o	o
6	EG	◎	◎	◎
	GI	◎	o	o
	AL	◎	◎	o
7	EG	o	o	o
	GI	o	o	o
	AL	o	o	o
8	EG	◎	◎	o
	GI	o	o	o
	AL	◎	o	o

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Table 5 (continued)

No.	Metal sheet	Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
5	9 EG		o	
	9 GI	o	o	o
	9 AL	o	o	o
10	10 EG	◎	◎	◎
	10 GI	◎	o	o
	10 AL	◎	◎	◎
15	11 EG	◎	◎	o
	11 GI	o	o	o
	11 AL	◎	o	o
20	12 EG	◎	◎	o
	12 GI	o	o	o
	12 AL	◎	o	o
25	13 EG	◎	◎	◎
	13 GI	◎	◎	◎
	13 AL	◎	◎	◎
30	14 EG	◎	◎	◎
	14 GI	o	o	o
	14 AL	◎	o	o
35	Comp. Ex. EG	o	△	△
	Comp. Ex. GI	△	△	x
	Comp. Ex. AL	o	△	△

Table 6

No.	Metal sheet	Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
40	15 EG	o	o	o
	15 GI	o	o	o
	15 AL	o	o	o
45	16 EG	◎	◎	◎
	16 GI	◎	o	o
	16 AL	◎	◎	◎
50	17 EG	◎	◎	o
	17 GI	o	o	o
	17 AL	◎	o	o

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Table 6 (continued)

No.	Metal sheet	Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
5	18 EG	◎	◎	○
	GI	○	○	○
	AL	◎	○	○
10	19 EG	◎	◎	◎
	GI	◎	◎	◎
	AL	◎	◎	◎
15	20 EG	◎	◎	◎
	GI	○	○	○
	AL	◎	○	○
20	21 EG	○	◎	○
	GI	○	○	○
	AL	○	○	○
25	22 EG	◎	◎	◎
	GI	◎	○	○
	AL	◎	◎	◎
30	23 EG	◎	◎	○
	GI	○	○	○
	AL	◎	○	○
35	24 EG	◎	◎	○
	GI	○	○	○
	AL	◎	○	○
40	25 EG	◎	◎	◎
	GI	◎	◎	◎
	AL	◎	◎	◎
45	26 EG	◎	◎	◎
	GI	○	○	○
	AL	◎	○	○

Table 7

No.	Metal sheet	Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
50	27 EG	◎	◎	◎
	GI	◎	○	○
	AL	◎	○	○
55				

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Tabl 7 (continued)

No.	Metal sheet	Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
5	28 EG	◎		○
	GI	◎	○	○
	AL	◎	○	○
10	29 EG	○	○	○
	GI	○	○	○
	AL	○	○	○
15	30 EG	◎	◎	◎
	GI	◎	○	○
	AL	◎	◎	◎
20	31 EG	◎	◎	◎
	GI	○	○	◎
	AL	○	○	○
25	32 EG	◎	◎	◎
	GI	◎	○	○
	AL	◎	◎	○
30	33 EG	○	○	○
	GI	○	○	○
	AL	○	○	○
35	34 EG	◎	◎	○
	GI	○	○	○
	AL	◎	○	○
40	35 EG	○	○	○
	GI	○	○	○
	AL	○	○	○
45	36 EG	◎	◎	◎
	GI	◎	○	○
	AL	◎	◎	◎
50	37 EG	◎	◎	○
	GI	○	○	○
	AL	◎	○	○
55	38 EG	◎	◎	○
	GI	○	○	○
	AL	◎	○	○
	39 EG	◎	◎	◎
	GI	◎	◎	◎
	AL	◎	◎	◎

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Table 7 (continued)

No.	Metal sheet	Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
5	40 EG	◎	◎	
	GI	○	○	○
	AL	◎	○	○

10

Table 8

No.	Metal sheet	Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
15	41 EG	○	○	○
	GI	○	○	○
	AL	○	○	○
20	42 EG	◎	◎	◎
	GI	◎	○	○
	AL	◎	◎	◎
25	43 EG	◎	◎	○
	GI	○	○	○
	AL	◎	○	○
30	44 EG	◎	◎	◎
	GI	○	○	○
	AL	◎	○	○
35	45 EG	◎	◎	◎
	GI	◎	◎	◎
	AL	◎	◎	◎
40	46 EG	◎	◎	◎
	GI	○	○	○
	AL	◎	○	○
45	47 EG	○	◎	○
	GI	○	○	○
	AL	○	○	○
50	48 EG	◎	◎	◎
	GI	◎	○	○
	AL	◎	◎	◎
55	49 EG	◎	◎	○
	GI	○	○	○
	AL	◎	○	○

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Table 8 (continued)

No.	Metal sheet	Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
5	50 EG	◎	◎	
	50 GI	○	○	○
	50 AL	◎	○	○
10	51 EG	◎	◎	◎
	51 GI	◎	◎	◎
	51 AL	◎	◎	◎
15	52 EG	◎	◎	◎
	52 GI	○	○	○
	52 AL	◎	○	○

20

Table 9

No.	Metal sheet	Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
25	53 EG	◎	◎	◎
	53 GI	◎	○	○
	53 AL	◎	○	○
30	54 EG	◎	○	○
	54 GI	◎	○	○
	54 AL	◎	○	○
35	55 EG	○	○	○
	55 GI	○	○	○
	55 AL	○	○	○
40	56 EG	◎	◎	◎
	56 GI	◎	○	○
	56 AL	◎	◎	◎
45	57 EG	◎	◎	◎
	57 GI	○	○	○
	57 AL	○	○	○
50	58 EG	◎	◎	◎
	58 GI	◎	○	○
	58 AL	◎	◎	○
55	59 EG	○	○	○
	59 GI	○	○	○
	59 AL	○	○	○

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Table 9 (continued)

No.	Metal sheet	Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
5	60 EG	◎	◎	
	GI	○	○	○
	AL	◎	○	○
10	61 EG	○	○	○
	GI	○	○	○
	AL	○	○	○
15	62 EG	◎	◎	◎
	GI	◎	○	○
	AL	◎	◎	◎
20	63 EG	◎	◎	◎
	GI	○	○	○
	AL	◎	○	○
25	64 EG	◎	◎	○
	GI	○	○	○
	AL	◎	○	○
30	65 EG	◎	◎	◎
	GI	◎	◎	◎
	AL	◎	◎	◎
35	66 EG	◎	◎	◎
	GI	○	○	○
	AL	◎	○	○

Table 10

No.	Metal sheet	Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
40	67 EG	○	○	○
	GI	○	○	○
	AL	○	○	○
45	68 EG	◎	◎	◎
	GI	◎	○	○
	AL	◎	◎	◎
50	69 EG	◎	◎	○
	GI	○	○	○
	AL	◎	○	○

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Table 10 (continued)

No.	Metal sheet	Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
5	70 EG	◎	◎	
	GI	○	○	○
	AL	◎	○	○
10	71 EG	◎	◎	◎
	GI	◎	◎	◎
	AL	◎	◎	◎
15	72 EG	◎	○	◎
	GI	○	○	○
	AL	◎	○	○
20	73 EG	○	◎	○
	GI	○	○	○
	AL	○	○	○
25	74 EG	◎	◎	◎
	GI	◎	○	○
	AL	◎	◎	◎
30	75 EG	◎	◎	○
	GI	○	○	○
	AL	◎	○	○
35	76 EG	◎	◎	◎
	GI	○	○	○
	AL	◎	○	○
40	77 EG	◎	◎	◎
	GI	◎	◎	◎
	AL	◎	◎	◎
45	78 EG	◎	◎	◎
	GI	○	○	○
	AL	◎	○	○

Table 11

No.	Metal sheet	Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
50	79 EG	◎	◎	◎
	GI	◎	○	○
	AL	◎	○	○

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Table 11 (continued)

No.	Metal sheet	Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
5	80 EG	◎	○	○
	80 GI	◎	○	○
	80 AL	◎	○	○
10	81 EG	○	○	○
	81 GI	○	○	○
	81 AL	○	○	○
15	82 EG	◎	◎	◎
	82 GI	◎	○	○
	82 AL	◎	◎	◎
20	83 EG	◎	◎	◎
	83 GI	○	○	○
	83 AL	○	○	○
25	84 EG	◎	◎	◎
	84 GI	◎	○	○
	84 AL	◎	◎	○
30	85 EG	○	○	○
	85 GI	○	○	○
	85 AL	○	○	○
35	86 EG	◎	◎	○
	86 GI	○	○	○
	86 AL	◎	○	○
40	87 EG	○	○	○
	87 GI	○	○	○
	87 AL	○	○	○
45	88 EG	◎	◎	◎
	88 GI	◎	○	○
	88 AL	◎	◎	◎
50	89 EG	◎	◎	○
	89 GI	○	○	○
	89 AL	◎	○	○
55	90 EG	◎	◎	○
	90 GI	○	○	○
	90 AL	◎	○	○
55	91 EG	◎	◎	◎
	91 GI	◎	◎	◎
	91 AL	◎	◎	◎

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Table 11 (continued)

No.	Metal sheet	Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
5	92 EG	◎	◎	◎
	GI	○	○	○
	AL	◎	○	○

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Table 12

No.	Metal sheet	Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
15	93 EG	○	○	○
	GI	○	○	○
	AL	○	○	○
20	94 EG	◎	◎	◎
	GI	◎	○	○
	AL	◎	◎	◎
25	95 EG	◎	◎	○
	GI	○	○	○
	AL	◎	○	○
30	96 EG	◎	◎	○
	GI	○	○	○
	AL	◎	○	○
35	97 EG	◎	◎	◎
	GI	◎	◎	◎
	AL	◎	◎	◎
40	98 EG	◎	◎	◎
	GI	○	○	○
	AL	◎	○	○
45	99 EG	○	◎	○
	GI	○	○	○
	AL	○	○	○
50	100 EG	◎	◎	◎
	GI	◎	○	○
	AL	◎	◎	◎
55	101 EG	◎	◎	○
	GI	○	○	○
	AL	◎	○	○

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Table 12 (continued)

No.	Metal sheet	Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
5	102 EG	◎	◎	
	GI	○	○	○
	AL	◎	○	○
10	103 EG	◎	◎	◎
	GI	◎	◎	◎
	AL	◎	◎	◎
15	104 EG	◎	◎	◎
	GI	○	○	○
	AL	◎	○	○

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Table 13

No.	Lanthanum oxide (g)	85% phosphoric acid (g)	Organic-based corrosion inhibitor	Metal sheet	Performance evaluation		
					Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
151	32.6	115.3	butyl thio-glycolate 1.0 g	EG	o	•	o
				GI	o	o	o
				AL	o	o	o
152	32.6	115.3	octyl thio-glycolate 1.0 g	EG	•	•	•
				GI	•	o	o
				AL	•	o	o
153	32.6	115.3	stearyl thio-glycolate 1.0 g	EG	•	•	•
				GI	•	o	o
				AL	•	o	o
154	32.6	115.3	α -mercapto-caproic acid 1.0 g	EG	•	•	o
				GI	•	o	o
				AL	•	o	o
155	32.6	115.3	8-mercapto-quinoline 1.0 g	EG	•	•	o
				GI	o	o	o
				AL	o	o	o
156	32.6	115.3	8-hydroxy quinoline 1.0 g	EG	•	•	•
				GI	•	•	o
				AL	•	•	•
157	32.6	115.3	6-(N,N'-dibutylamino-1,3,5-triazine-2,4-dithiol 1.0 g	EG	o	o	o
				GI	o	o	o
				AL	o	o	o
158	32.6	115.3	lauryl gallate 1.0 g	EG	•	•	•
				GI	o	o	o
				AL	•	•	o

Table 13 (Cont.)

No.	Lanthanum oxide (g)	85% phosphoric acid (g)	Organic-based corrosion inhibitor	Metal sheet	Performance evaluation		
					Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
159	32.6	115.3	1 wt% aqueous polyaniline solution (dopant: barium sulfate) 1.0 g	EG	0	0	0
				GI	0	0	0
				AL	0	0	0
160	32.6	115.3	N-phenyl-3-formyl-2,5-dimethyl-pyrrole 1.0 g	EG	•	•	•
				GI	•	•	•
				AL	•	•	•
161	32.6	115.3	α -mercapto-lauric acid 1.0 g	EG	•	•	•
				GI	0	0	0
				AL	•	0	0
162	32.6	115.3	α -mercapto-lauric acid 0.1 g	EG	•	0	0
				GI	0	0	0
				AL	•	0	0
163	32.6	115.3	α -mercapto-lauric acid 10.0 g	EG	•	•	•
				GI	•	0	0
				AL	•	•	0
164	32.6	115.3	nicotinic acid 1.0 g	EG	•	•	•
				GI	•	•	•
				AL	•	•	•
165	32.6	115.3	catechol 1.0 g	EG	•	•	•
				GI	•	•	•
				AL	•	•	•

Table 14

No.	Lanthanum oxide (g)	85% phosphoric acid (g)	α -mercaptop-tolauric acid (g)	Added aid	Metal sheet	Performance evaluation					
						Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance			
166	32.6	115.3	1.0	cerium oxide 3.4 g	EG	◎	◎	◎			
					GI	○	○	○			
					AL	◎	◎	◎			
167	32.6	115.3	1.0	cerium hydroxide 4.2 g	EG	○	○	○			
					GI	○	○	○			
					AL	○	○	○			
168	32.6	115.3	1.0	cerium chloride $\cdot 7H_2O$ 7.5 g	EG	◎	◎	◎			
					GI	○	◎	◎			
					AL	◎	◎	◎			
169	32.6	115.3	1.0	cerium chloride $\cdot 8H_2O$ 6.0 g	EG	◎	◎	◎			
					GI	○	◎	◎			
					AL	○	○	○			
170	32.6	115.3	1.0	cerium sulfate $\cdot 6H_2O$ 14.3 g	EG	◎	◎	◎			
					GI	○	◎	◎			
					AL	○	○	○			
171	32.6	115.3	1.0	cerium nitrate $\cdot 6H_2O$ 8.7 g	EG	◎	◎	◎			
					GI	○	○	○			
					AL	○	○	○			
172	32.6	115.3	1.0	cerium acetate $\cdot H_2O$ 6.7 g	EG	◎	◎	◎			
					GI	○	○	○			
					AL	○	○	○			
173	32.6	115.3	1.0	cerium phosphate 4.7 g	EG	◎	◎	◎			
					GI	○	○	○			
					AL	○	○	○			
Comp. Ex.	Application chromate film					EG	○	△			
						GI	△	△			
						AL	○	△			

Table 15

No.	Film composition			Metal sheet	Performance evaluation		
	Cerium phosphate (g)	85% phosphoric acid (g)	Organic-based corrosion inhibitor		Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
174	23.5	115.3	butyl thioglycolate 1.0 g	EG	⊕	⊕	⊕
				GI	⊕	○	○
				AL	⊕	○	○
175	23.5	115.3	octyl thioglycolate 1.0 g	EG	⊕	⊕	⊕
				GI	⊕	○	○
				AL	⊕	○	○
176	23.5	115.3	stearyl thioglycolate 1.0 g	EG	○	○	○
				GI	○	○	○
				AL	○	○	○
177	23.5	115.3	α -mercapto-caproic acid 1.0 g	EG	⊕	⊕	⊕
				GI	⊕	○	○
				AL	⊕	○	○
178	23.5	115.3	8-mercapto-quinoline 1.0 g	EG	⊕	⊕	⊕
				GI	○	○	○
				AL	○	○	○
179	23.5	115.3	8-hydroxy quinoline 1.0 g	EG	⊕	⊕	⊕
				GI	⊕	○	○
				AL	⊕	⊕	○
180	23.5	115.3	6-(N,N'-dibutylamino)-1,3,5-triazine-2,4-dithiol 1.0 g	EG	○	○	○
				GI	○	○	○
				AL	○	○	○
181	23.5	115.3	lauryl gallate 1.0 g	EG	⊕	⊕	○
				GI	○	○	○
				AL	⊕	○	○

Table 15 (Cont.)

No.				Metal sheet	Performance evaluation		
	Cerium phosphate (g)	85% phosphoric acid (g)	Organic-based corrosion inhibitor		Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
182	23.5	115.3	1 wt% aqueous polyaniline solution (dopant: barium sulfate) 1.0 g	EG	o	o	o
				GI	o	o	o
				AL	o	o	o
183	23.5	115.3	N-phenyl-3-formyl-2,5-dimethyl-pyrrole 1.0 g	EG	•	•	o
				GI	o	o	o
				AL	•	o	o
184	23.5	115.3	α -mercapto-lauric acid 1.0 g	EG	•	•	o
				GI	o	o	o
				AL	•	o	o
185	23.5	115.3	α -mercapto-lauric acid 0.1 g	EG	•	•	•
				GI	•	•	•
				AL	•	•	•
186	23.5	115.3	α -mercapto-lauric acid 10.0 g	EG	•	•	•
				GI	o	o	o
				AL	•	o	o
187	23.5	115.3	nicotinic acid 1.0 g	EG	•	•	•
				GI	•	•	•
				AL	•	•	•
188	23.5	115.3	catechol 1.0 g	EG	•	•	•
				GI	•	•	•
				AL	•	•	•

Table 16

No.		Film composition			Metal sheet	Performance evaluation		
	Cerium phosphate (g)	85% phosphoric acid (g)	α -mercaptoauric acid (g)	Added aid		Working follow-up property	Flat sheet corrosion resistance	Worked part corrosion resistance
189	23.5	115.3	1.0	cerium oxide 3.4 g	EG	◎	◎	◎
					Gl	○	○	○
					AL	◎	○	○
190	23.5	115.3	1.0	cerium hydroxide 4.2 g	EG	◎	◎	◎
					Gl	○	○	○
					AL	◎	○	○
191	23.5	115.3	1.0	cerium chloride • 7H ₂ O 7.5 g	EG	◎	◎	◎
					Gl	○	◎	○
					AL	◎	○	◎
192	23.5	115.3	1.0	cerium chloride • 8H ₂ O 6.0 g	EG	◎	◎	◎
					Gl	○	○	○
					AL	◎	○	◎
193	23.5	115.3	1.0	cerium sulfate • 6H ₂ O 14.3 g	EG	◎	◎	◎
					Gl	○	○	○
					AL	◎	○	◎
194	23.5	115.3	1.0	cerium nitrate • 6H ₂ O 8.7 g	EG	◎	◎	◎
					Gl	○	◎	○
					AL	◎	○	◎
195	23.5	115.3	1.0	cerium acetate • H ₂ O 6.7 g	EG	◎	◎	◎
					Gl	○	○	○
					AL	◎	○	◎
Comp. Ex.	Application chromate film				EG	○	△	△
					Gl	△	△	×
					AL	○	△	△

Example 7

[0073] The basic effect of the surface treatment agent of the invention will now be illustrated concretely with simplified examples. A surface treatment agent containing as a lanthanum compound lanthanum phosphate obtained by reaction between lanthanum oxide and ortho-phosphoric acid, with 5 moles of ortho-phosphoric acid in terms of H₃PO₄ as the molar ratio with respect to the lanthanum, and with a lanthanum concentration of 0.64 mol/kg, with water as the diluting agent, was used to coat high purity zinc to obtain a coating layer with a thickness of about 5 μm . Fig. 2 shows an anode current-current curve for coated zinc and zinc with no coating layer in a 0.1 mol/liter NaCl solution adjusted to pH 8.4 with boric acid and sodium borate. The anode current for the zinc with the coating layer was notably smaller compared to the zinc with no coating layer, thus confirming an effect of suppressing anode elution of zinc in the coating layer and of inhibiting diffusion of chloride ion, a corrosion-accelerating substance, into the zinc surface.

Example 8

[0074] Fig. 3 shows an anode current-current curve obtained by exactly the same treatment as in Example 7, except that trivalent cerium oxide was used instead of lanthanum oxide as the lanthanum compound. The same results were obtained as in Example 7.

[Examples 9-10]

(Preparation of surface treatment agents)

10 Example 9

[0075] Surface treatment agents composed mainly of phosphoric acid and lanthanum phosphate, hydrogen phosphate, oxide, hydroxide or a mixture thereof.

[0076] A starting material lanthanum compound such as lanthanum oxide (a), lanthanum hydroxide (b), lanthanum chloride (c), etc. was reacted with ortho-phosphoric acid (d) or poly-phosphoric acid (e) to obtain the lanthanum compound for the surface treatment agent. Also, a phosphoric acid such as ortho-phosphoric acid, poly-phosphoric acid or meta-phosphoric acid (f) or a mixture thereof, and/or a phosphate salt such as ammonium phosphate (g) were further added to adjust the molar ratio of H_3PO_4 to lanthanum to the prescribed value. Water or a mixture of water and methanol (h) was added as a diluting agent to the resulting composition of the lanthanum compound and phosphoric acid, to obtain a surface treatment agent with the prescribed lanthanum concentration. Table 17 lists the surface treatment agents of samples No. 201-217 in the order of their phosphoric acid to lanthanum molar ratios, and the method of preparation is indicated as (a) to (h). For samples No.201 and No.210 only, a mixture of water and methanol was used as the diluting agent, in a weight proportion of 2:1 for both cases.

[0077] When a cerium compound and/or an organic-based corrosion inhibitor are added, they are added during addition of the phosphate after adjustment of the lanthanum compound, or simultaneously with the diluting agent. Of samples No. 281-224 listed in Table 18, samples No. 218-221 were specified as treatment agents with the same lanthanum compound and phosphoric acid composition as sample No.7, i.e. treatment agents with a lanthanum compound concentration of 0.3 mol/kg and ortho-phosphoric acid in a molar ratio of 5 with respect to lanthanum, and a cerium compound and/or an organic-based corrosion inhibitor were added. Also, samples No. 222-224 were specified as treatment agents with the same lanthanum compound and phosphoric acid composition as sample No.210, i.e. treatment agents with a lanthanum compound concentration of 0.5 mol/kg and poly-phosphoric acid in a molar ratio of 10 in terms of H_3PO_4 with respect to lanthanum, and cerium nitrate as a cerium compound and/or an organic inhibitor were added.

35 Example 10

[0078] Surface treatment agents composed mainly of phosphoric acid and cerium phosphate, hydrogen phosphate, oxide, hydroxide or a mixture thereof.

[0079] The starting material cerium compounds such as trivalent cerium oxide Ce_2O_3 (i), tetravalent cerium oxide CeO_2 (j), trivalent cerium hydroxide (k), trivalent cerium chloride (l) and cerium sulfate (m) were reacted with ortho-phosphoric acid (n) or poly-phosphoric acid (o) to obtain cerium compounds for the surface treatment agents. Also, a phosphoric acid such as ortho-phosphoric acid, poly-phosphoric acid or meta-phosphoric acid (p) or a mixture thereof, and/or a phosphate salt such as ammonium phosphate (g) were further added to adjust the molar ratio of H_3PO_4 to cerium to the prescribed value. Water or a mixture of water and methanol (r) was added as a diluting agent to the resulting composition of the cerium compound and phosphoric acid, to obtain a surface treatment agent with the prescribed cerium concentration. Table 19 lists the surface treatment agents of samples No. 225-241 in the order of their phosphoric acid to cerium molar ratios, and the method of preparation is indicated as (i) to (r). For samples No.225 and No.234 only, a mixture of water and methanol was used as the diluting agent, in a weight proportion of 2:1 for both cases.

[0080] When a lanthanum compound and/or an organic-based corrosion inhibitor are added, they are added during addition of the phosphate after adjustment of the cerium compound, or simultaneously with the diluting agent. Of samples No. 242-248 listed in Table 20 samples No. 242-245 were specified as treatment agents with the same cerium compound and phosphoric acid composition as sample No.231, i.e. treatment agents with a cerium compound concentration of 0.3 mol/kg and ortho-phosphoric acid in a molar ratio of 5 with respect to cerium, and a lanthanum compound and/or an organic-based corrosion inhibitor were added. Also, samples No. 246-248 were specified as treatment agents with the same cerium compound and phosphoric acid composition as sample No.234, i.e. treatment agents with a cerium compound concentration of 0.5 mol/kg and poly-phosphoric acid in a molar ratio of 10 in terms of H_3PO_4 with respect to cerium, and lanthanum chloride as a lanthanum compound and/or an organic-based corrosion inhibitor were

added.

[0081] The organic inhibitors used in Tabl 2 are indicated by the following abbreviations.

PFDP:	N-phenyl-3-formyl-2,5-dimethylpyrrole
TGO:	octyl thioglycolate
MLA:	α -mercaptoplauric acid
MBA:	α -mercaptopbenzoic acid
MNA:	α -mercaptopnicotinic acid
HOQ:	8-hydroxyquinoline

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(Film-forming method)

[0082] The film-forming method for the treatment agents with a low degree of dilution, and hence a high viscosity, was application with a bar coater to a dry coating layer thickness of 1 μm . For the treatment agents with a high degree of dilution and hence a low viscosity, spreading was accomplished by spraying to a dry coating layer thickness of 0.2 μm . After the coating or spreading, the metal material was heat treated at 100-200°C for 30 seconds to one hour. Formation of the coating layer by dipping was accomplished by holding the metal material in the treatment bath at 85°C for 30 seconds, and drying in air. The metal sheet used was GI (fused zinc-plated steel sheet, plating coverage: 90 g/m²), EG (zinc-electroplated steel sheet, plating coverage: 20 g/m²) or AL (fused aluminum-silicon alloy-plated steel sheet, plating coverage: 120 g/m², Al/Si = 90/10) plated steel sheets, cold-rolled steel sheets and aluminum sheets.

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[0083] In Comparative Example 201, for comparison with zinc phosphate surface treatment agents containing lanthanum compounds, GI and EG were used as the metal materials and dipped for 2 minutes at 40°C in a treatment solution comprising 0.01 mol/kg of lanthanum nitrate in terms of lanthanum, and ortho-phosphoric acid at a molar ratio of 15 in terms of H₃PO₄ to lanthanum, and water washing was followed by drying at 100°C for 10 minutes to form films.

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[0084] In Comparative Example 203, for comparison with a cathode-deposited cerium compound, EG was used as the metal material and a cathode current was passed through at a current density of 100 mA/cm² in a 0.1 mol/liter trivalent cerium chloride solution to deposit trivalent cerium hydroxide on the surface, after which reaction with ortho-phosphoric acid gave a mixed film of cerium phosphate and hydroxide compounds.

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[0085] In Comparative Example 202, for comparison with chromate treatment, a treatment bath was prepared containing 30 g/l of chromic acid partially reduced with starch in terms of CrO₃, 40 g/l of SiO₂ and 20 g/l of phosphoric acid, and films were formed by application, drying and hardening onto steel sheets. (The amount of Cr in the films was 120 mg/m² in terms of Cr metal).

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[0086] In Comparative Example 203, for comparison with a cathode-deposited cerium compound, EG was used as the metal material and a cathode current was passed through at a current density of 100 mA/cm² in a 0.1 mol/liter trivalent cerium chloride solution to deposit trivalent cerium hydroxide on the surface, after which reaction with ortho-phosphoric acid gave a mixed film of cerium phosphate and hydroxide compounds.

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[0087] Incidentally, for the metal materials and film-forming methods listed in Tables 17-20, the plated steel sheets used as metal materials are indicated by type as GI, EG or AL, and the coating methods for forming the films are indicated by (P), (S) or (D) for painting, spraying or dipping, respectively. (Evaluation of coating layer performance)

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[0088] The method of performance evaluation was the same as for Examples 1-6.

[0089] The relationship between the surface treatment agent compositions and their evaluation results are shown in Tables 17-20. As clearly seen in Tables 17 and 19, the metal material surface treatment agents of the invention composed mainly of lanthanum compounds or cerium compounds and phosphoric acid provide coating layers with excellent working follow-up properties and corrosion resistance, and with rust prevention with the films alone which has not been

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achieved with conventional zinc phosphate treatment, while also providing coating layers with flat and worked part corrosion resistance equivalent to that achieved with chromate treatment. They therefore provide a means of forming films as conversion treatment films containing absolutely no hexavalent chromium, and exhibiting excellent environmental suitability with their effect as anti-corrosion films. In addition, as clearly seen in Tables 18 and 20, the lanthanum compounds or cerium compounds and the organic-based corrosion inhibitors have the effect of complementing the corrosion resistance, especially the worked part corrosion resistance, of coating layers formed from surface treatment agents composed mainly of cerium compounds or lanthanum compounds and phosphoric acid, and therefore a means is provided for reinforcing their effect as anti-corrosion films containing no hexavalent chromium.

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Table 17

Sample No.	Treatment agent		Metal material and film forming method	Worked part follow-up property	Corrosion resistance	
	Phosphoric acid molar ratio	Lanthanum concentration (mol/kg)			Flat parts	Worked parts
201	1.0(d)	2.4(a,h)	GI(P)	o	o	o
202	1.0(d)	1.5(a)	GI(P)	o	o	o
203	3.0(d)	1.05(a)	GI(P)	o	o	o
			EG(P)	o	◎	o
			AL(P)	o	o	o
204	3.0(d)	0.5(a)	GI(P)	◎	o	o
			EG(P)	◎	◎	o
			AL(P)	◎	o	o
205	4.0(e)	1.0(a)	GI(P)	◎	◎	◎
			EG(P)	◎	◎	◎
			AL(P)	◎	◎	◎
206	5.0(d)	0.64(a)	GI(P)	◎	◎	◎
207	5.0(d)	0.3(a)	GI(P)	◎	o	o
			EG(P)	◎	◎	o
			AL(P)	◎	o	o
			cold-rolled steel sheet (P)	-	o	-
			aluminum sheet (P)	-	o	-
208	5.0(d,f)	0.3(a)	GI(P)	o	o	o
209	5.0(d,g)	0.3(a)	EG(P)	o	o	o
210	10 (e)	0.5(a)	GI(P)	◎	◎	o
211	10 (e,f)	0.5(b,c)	EG(P)	◎	◎	o
212	10 (e,f)	0.5(c)	EG(P)	◎	◎	o
213	10 (e)	0.2(c)	GI(S)	◎	o	o
214	10 (e,f)	0.2(c,h)	GI(S)	◎	o	o
			EG(S)	◎	o	o
			AL(S)	◎	o	o
215	10 (e,f)	0.1	EI(S)	◎	o	o
216	10 (e)	0.06(a)	GI(D)	o	o	o
217	25 (d)	0.11(c)	GI(D)	o	o	△
			EG(D)	o	o	△

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Table 17 (continued)

Sample No.	Treatment agent		Metal material and film forming method	Worked part follow-up property	Corrosion resistance	
	Phosphoric acid molar ratio	Lanthanum concentration (mol/kg)			Flat parts	Worked parts
Comp. Ex. 201	15 (d)	0.01	GI(D)	△	x	x
			EG(D)	△	x	x
202	chromate treated	-	GI(P)	△	o	△
			EG(P)	o	o	△
			AL(P)	o	o	△

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Table 18

Sample No.	Cerium compound and molar ratio to La	Organic inhibitor and molar ratio to La	Metal material and film forming method	Worked part follow-up property	Corrosion resistance	
					Flat parts	Worked parts
218	CePO ₄ 1.0	none	GI(P)	◎	◎	o
	CePO ₄ 1.0	PFDP 0.01	GI(P)	◎	◎	◎
	CePO ₄ 1.0	TGO 0.01	GI(P)	◎	◎	o
	CePO ₄ 1.0	MLA 0.01	GI(P)	◎	◎	o
	CePO ₄ 1.0	MBA 0.01	GI(P)	◎	◎	◎
	CePO ₄ 1.0	MNA 0.01	GI(P)	◎	◎	◎
	CePO ₄ 1.0	HOQ 0.01	GI(P)	◎	◎	o
219	none	PFDP 0.5	GI(P)	◎	◎	o
220	CeO ₂ 0.01	none	GI(P)	◎	◎	o
221	Ce(OH) ₃ 0.01	none	GI(P)	◎	◎	o
222	Ce(NO ₃) ₃ 0.5	none	GI(P)	◎	◎	◎
			EG(P)	◎	◎	◎
			AL(P)	◎	◎	◎
223	Ce(NO ₃) ₃ 0.3	PFDP 0.2	GI(P)	◎	◎	◎
			EG(P)	◎	◎	◎
			AL(P)	◎	◎	◎
224	Ce(NO ₃) ₃ 0.3	MNA 0.2	GI(P)	◎	◎	◎
			EG(P)	◎	◎	◎
			AL(P)	◎	◎	◎

Table 19

	Sample No.	Treatment	agent	Metal material and film forming method	Worked part follow-up property	Corrosion resistance	
5		Phosphoric acid molar ratio	Cerium concentration (mol/kg)			Flat parts	Worked parts
10	225	0.8(n)	2.4(i,r)	GI(P)	△	○	△
15	226	1.0(n)	1.5(j)	GI(P)	○	○	○
20	227	3.0(n)	1.05(j)	GI(P)	○	○	○
25				EG(P)	○	○	○
30				AL(P)	○	○	○
35	228	3.0(n)	0.5(k)	GI(P)	○	○	○
40				EG(P)	○	◎	○
45				AL(P)	○	○	○
50	229	4.0(o)	1.0(k)	GI(P)	○	◎	○
55	230	5.0(n)	0.64(j)	EG(P)	○	◎	○
60				AL(P)	○	◎	○
65				GI(P)	○	◎	○
70				EG(P)	○	○	○
75				AL(P)	○	○	○
80	231	5.0(n)	0.3(j)	cold-rolled steel sheet (P)	-	○	-
85				aluminum sheet (P)	-	○	-
90	232	5.0(n,p)	0.3(j)	GI(P)	○	○	○
95	233	5.0(n,q)	0.3(j)	EG(P)	○	○	○
100	234	10 (o)	0.5(k)	GI(P)	◎	◎	○
105	235	10 (o)	0.5(k,l)	EG(P)	◎	◎	○
110	236	10 (o)	0.5(k,m)	EG(P)	◎	◎	○
115	237	10 (o)	0.2(k)	GI(S)	◎	○	○
120	238	10 (o)	0.2(k,r)	EG(S)	◎	○	○
125	239	10 (o)	0.1(j)	GI(D)	○	○	○
130	240	10 (n)	0.06(j)	GI(D)	○	○	△
135	241	25 (n)	0.11(k)	EG(D)	○	○	△
140	Comp. Ex. 203	cathode deposition	-	EG	X	△	X

Table 20

Sample No.	Lanthanum compound and molar ratio to Ce	Organic-based corr - sion inhibitor and molar ratio to Ce	Metal material and film-forming method	Worked part follow-up property	Corrosion resistance	
					Flat parts	Worked parts
242	LaPO ₄ 0.8	none	GI(P)	◎	◎	○
	LaPO ₄ 0.8	PFDP 0.01	GI(P)	◎	◎	◎
	LaPO ₄ 0.8	TGO 0.01	GI(P)	◎	◎	○
	LaPO ₄ 0.8	MLA 0.01	GI(P)	◎	◎	○
	LaPO ₄ 0.8	MBA 0.01	GI(P)	◎	◎	◎
	LaPO ₄ 0.8	MNA 0.01	GI(P)	◎	◎	◎
	LaPO ₄ 0.8	HOQ 0.01	GI(P)	◎	◎	○
243	none	PFDP 0.5	GI(P)	○	◎	○
244	La ₂ O ₃ 0.01	none	GI(P)	○	◎	○
245	La(OH) ₃ 0.01	none	GI(P)	○	◎	○
246	LaCl ₃ 0.5	none	GI(P)	◎	◎	◎
			EG(P)	◎	◎	◎
			AL(P)	◎	◎	◎
247	LaCl ₃ 0.3	PFDP 0.2	GI(P)	◎	◎	◎
			EG(P)	◎	◎	◎
			AL(P)	◎	◎	◎
248	LaCl ₃ 0.3	MNA 0.2	GI(P)	◎	◎	◎
			EG(P)	◎	◎	◎
			AL(P)	◎	◎	◎

Claims

1. A surface treated metal material characterized by having a corrosion resistant coating layer composed mainly of an oxyacid compound or hydrogen oxyacid compound of a rare earth element, or a mixture thereof, on the surface of a metal material.
2. A surface treated metal material according to claim 1, wherein said rare earth element is yttrium, lanthanum and/or cerium.
3. A surface treated metal material according to claim 1 or claim 2, wherein the anion species of said oxyacid compound and said hydrogen oxyacid compound is a polyvalent oxyacid anion.
4. A surface treated metal material according to claim 3, wherein said anion species is phosphate ion, tungstate ion, molybdate ion and/or vanadate ion.
5. A surface treated metal material according to claim 1, wherein said corrosion resistant coating layer is composed mainly of a phosphate compound or hydrogen phosphate compound of yttrium, lanthanum and/or cerium, or a mixture thereof.

6. A surface treated metal material according to claim 5, wherein said phosphate compound and said hydrogen phosphate compound is an ortho-(hydrogen) phosphate compound, meta-phosphate compound or poly-(hydrogen)phosphate compound, or a mixture thereof.
- 5 7. A surface treated metal material according to any of claims 1 to 6, wherein said corrosion resistant coating layer further contains as an added component one or more compounds selected from among oxides, hydroxides, halides and organic acid compounds of rare earth elements.
- 10 8. A surface treated metal material according to claim 7, wherein said rare earth element of said added component is cerium.
9. A surface treated metal material according to claim 8, wherein said rare earth element of said added component is tetravalent cerium.
- 15 10. A surface treated metal material according to any of claims 1 to 9, wherein said corrosion resistant coating further contains as an added component an organic-based corrosion inhibitor.
- 20 11. A surface treated metal material according to claim 10, wherein said organic-based corrosion inhibitor is one or more compounds selected from the group consisting of formylated derivatives of N-phenyldimethylpyrrole, thioglycolic acid esters represented by $\text{HS}-\text{CH}_2\text{COOC}_n\text{CH}_{2n+1}$ (n is an integer of 1-25) and their derivatives, α -mercapto-carboxylic acids represented by $\text{C}_n\text{H}_{2n}(\text{SH})\text{COOH}$ (n is an integer of 1-25) and their derivatives, quinoline and its derivatives, triazinedithiol and its derivatives, gallic acid esters and their derivatives, nicotinic acid and its derivatives, catechol and its derivatives and/or conductive polymers.
- 25 12. A surface treated metal material according to any of claims 1 to 11, wherein said corrosion resistant coating layer further contains one or more compounds selected from the group consisting of SiO_2 , Cr_2O_3 , $\text{Cr}(\text{OH})_3$, Al_2O_3 , calcium hydroxide, calcium carbonate, calcium oxide, zinc phosphate, zinc hydrogen phosphate, potassium phosphate, potassium hydrogen phosphate, calcium phosphate, calcium hydrogen phosphate, calcium silicate, zirconium silicate, aluminum phosphate, aluminum hydrogen phosphate, titanium oxide, zirconium phosphate, zirconium hydrogen phosphate, sulfuric acid, sodium sulfate, sodium hydrogen sulfate, phosphoric acid, sodium phosphate and sodium hydrogen phosphate.
- 30 13. A surface treatment agent for forming corrosion resistant coating layers on the surfaces of metal materials, characterized by being composed mainly of an oxyacid compound or hydrogen oxyacid compound of a rare earth element, or a mixture thereof.
- 35 14. A surface treatment agent according to claim 13, wherein said rare earth element is yttrium, lanthanum and/or cerium.
- 40 15. A surface treatment agent according to claim 13 or 14, wherein the anion species of said oxyacid compound and said hydrogen oxyacid compound is a polyvalent oxyacid anion.
16. A surface treatment agent according to claim 15, wherein said anion species is phosphate ion, tungstate ion, molybdate ion and/or vanadate ion.
- 45 17. A surface treatment agent according to claim 13, wherein said corrosion resistant coating layer is composed mainly of a phosphate compound or hydrogen phosphate compound of yttrium, lanthanum and/or cerium, or a mixture thereof.
- 50 18. A surface treatment agent according to claim 17, wherein said phosphate compound and Said hydrogen phosphate compound is an ortho-(hydrogen)phosphate compound, meta-phosphate compound or poly-(hydrogen)phosphate compound, or a mixture thereof.
- 55 19. A surface treatment agent according to any of claims 13 to 18, wherein said corrosion resistant coating layer further contains as an added component one or more Compounds selected from among oxides, hydroxides, halides and organic oxyacid compounds of rare earth elements.
20. A surface treatment agent according to claim 19, wherein said rare earth element of said added component is

cerium.

21. A surface treatment agent according to claim 20, wherein said rare earth element of said added component is tetravalent cerium.

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22. A surface treatment agent according to any of claims 13 to 21, wherein said corrosion resistant coating further contains as an added component an organic-based corrosion inhibitor.

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23. A surface treatment agent according to claim 22, wherein said organic-based corrosion inhibitor is one or more compounds selected from the group consisting of formylated derivatives of N-phenyl-dimethylpyrrole, thioglycolic acid esters represented by $\text{HS}-\text{CH}_2\text{COOC}_n\text{CH}_{2n+1}$ (n is an integer of 1-25) and their derivatives, α -mercaptopcarboxylic acids represented by $\text{C}_n\text{H}_{2n}(\text{SH})\text{COOH}$ (n is an integer of 1-25) and their derivatives, quinoline and its derivatives, triazinedithiol and its derivatives, gallic acid esters and their derivatives, nicotinic acid and its derivatives, catechol and its derivatives and/or conductive polymers.

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24. A surface treatment agent according to any of claims 13 to 23, wherein said corrosion resistant coating layer further contains one or more compounds selected from the group consisting of SiO_2 , Cr_2O_3 , $\text{Cr}(\text{OH})_3$, Al_2O_3 , calcium hydroxide, calcium carbonate, calcium oxide, zinc phosphate, zinc hydrogen phosphate, potassium phosphate, potassium hydrogen phosphate, calcium phosphate, calcium hydrogen phosphate, calcium silicate, zirconium silicate, aluminum phosphate, aluminum hydrogen phosphate, titanium oxide, zirconium phosphate, zirconium hydrogen phosphate, sulfuric acid, sodium sulfate, sodium hydrogen sulfate, phosphoric acid, sodium phosphate and sodium hydrogen phosphate.

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25. A surface treatment agent characterized by containing 0.05-4 mol/kg of a rare earth compound in terms of the rare earth element, and 0.5-100 moles of a phosphate compound and/or hydrogen phosphate compound in terms of H_3PO_4 to one mole of the rare earth element.

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26. A surface treatment agent according to claim 25, wherein said rare earth element compound is a phosphate compound, hydrogen phosphate compound, oxide or hydroxide of lanthanum or cerium, or a mixture thereof.

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27. A surface treatment agent according to claim 25 or 26, wherein the phosphate is an ortho-phosphate, meta-phosphate or poly-phosphate, or a mixture thereof.

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28. A surface treatment agent according to any of claims 25 to 27, which contains water or a mixture of water and a water-soluble organic solvent as a diluting agent.

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29. A surface treatment agent according to any of claims 25 to 28, wherein said rare earth element compound is a lanthanum compound, and which further contains a cerium compound in a molar ratio of 1.0-0.001 in terms of cerium to lanthanum and/or an organic-based corrosion inhibitor in a molar ratio of 2-0.001 to lanthanum.

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Fig. 1

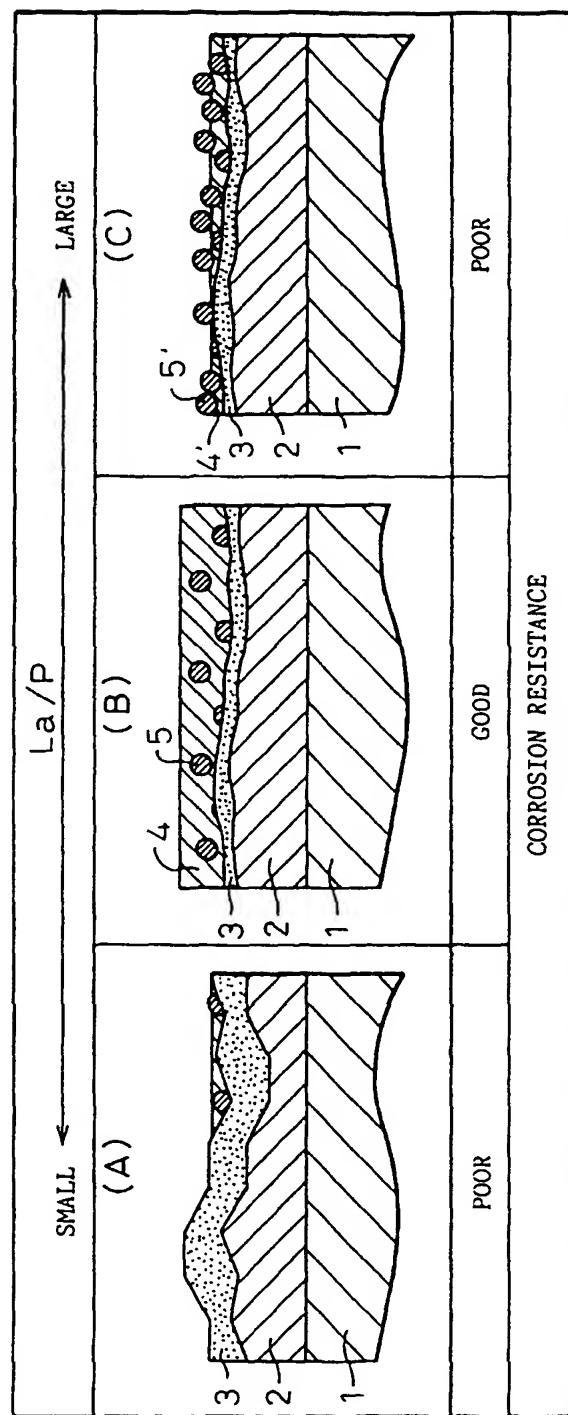


Fig. 2

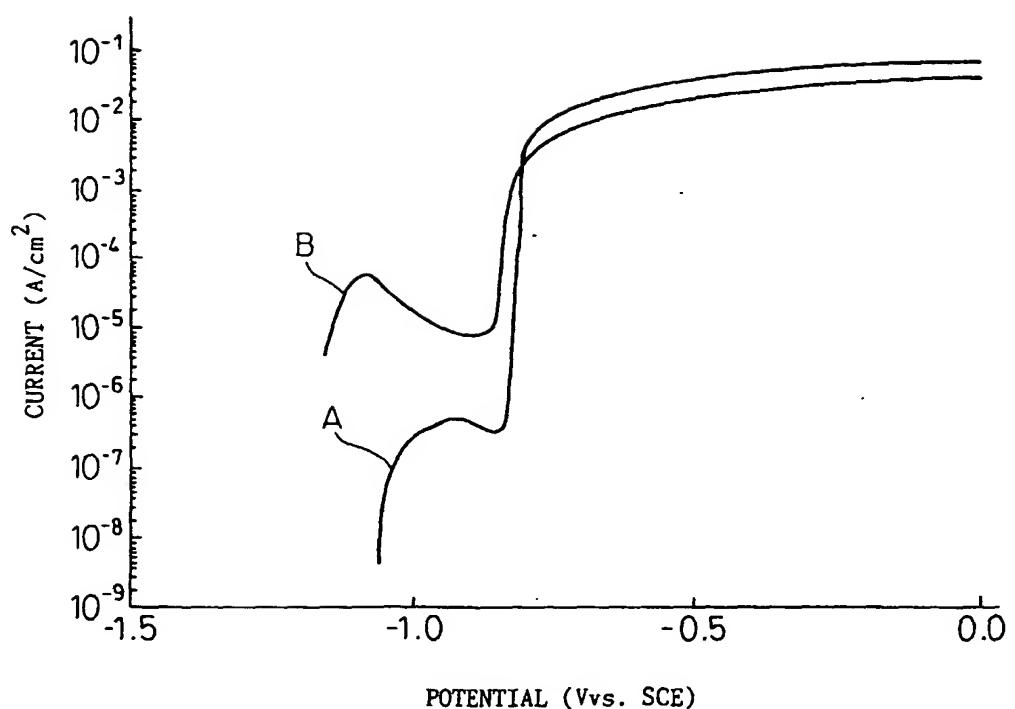
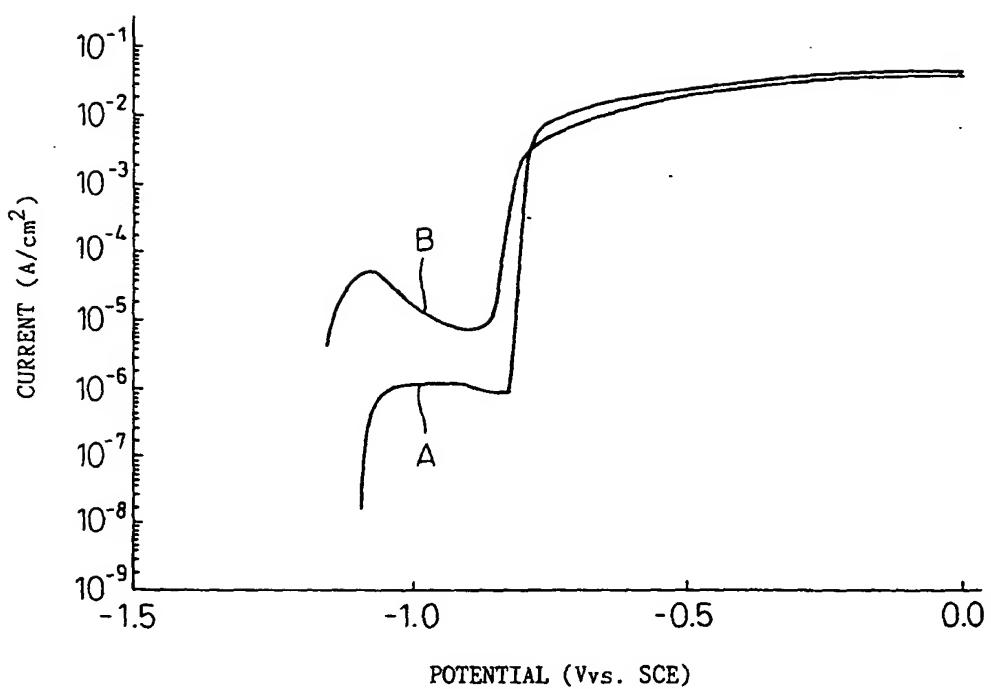


Fig. 3



INTERNATIONAL SEARCH REPORT		International application No. PCT/JP97/00272
A. CLASSIFICATION OF SUBJECT MATTER Int. Cl ⁶ C23C48, C23C22/07, C23C30/00		
According to International Patent Classification (IPC) or to both national classification and IPC		
B. FIELDS SEARCHED Minimum documentation searched (classification system followed by classification symbols) Int. Cl ⁶ C23C22/00-86, C23C24/00-30/00		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched Jitsuyo Shinan Koho 1926 - 1996 Jitsuyo Shinan Toroku Kokai Jitsuyo Shinan Koho 1971 - 1997 Koho 1996 - 1997 Toroku Jitsuyo Shinan Koho 1994 - 1997		
Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)		
C. DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	JP, 5-331658, A (Nippon Paint Co., Ltd.), December 14, 1993 (14. 12. 93), Claims 1 to 7; column 7, line 18 to column 8, line 7	1-7, 12-19, 24-28
Y	& EP, 564286, A2 & US, 5328526, A	10, 11, 22, 23
X	JP, 5-195247, A (Hughes Aircraft Co.), August 3, 1993 (03. 08. 93), Claims 1, 2	1-3, 7, 13-15, 19,
Y	& EP, 534120, A1 & US, 5192374, A	20-21 10, 11, 22, 23
X	JP, 3-64485, A (Nippon Paint Co., Ltd.), March 19, 1991 (19. 03. 91), Claims 1, 2; page 2, upper right column, line 16 to lower left column, line 3; page 3, upper left column, line 8 to page 4, upper left	1-7, 10, 12-19, 22, 24-30
Y	& EP, 411609, A & US, 5104577, A	10, 11, 22, 23
<input checked="" type="checkbox"/> Further documents are listed in the continuation of Box C. <input type="checkbox"/> See patent family annex.		
* Special categories of cited documents: "A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier document but published on or after the international filing date "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "O" document referring to an oral disclosure, use, exhibition or other means "P" document published prior to the international filing date but later than the priority date claimed		
Date of the actual completion of the international search April 23, 1997 (23. 04. 97)		Date of mailing of the international search report May 7, 1997 (07. 05. 97)
Name and mailing address of the ISA/ Japanese Patent Office Facsimile No.		Authorized officer Telephone No.

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INTERNATIONAL SEARCH REPORT

International application No.

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C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	JP, 2-25579, A (Nippon Paint Co., Ltd.), January 29, 1990 (29. 01. 90), Claims 1, 2; page 2, upper left column, line 18 to upper right column, line 1 & EP, 337075, A & US, 4992115, A	1-9, 12-21, 24-30 10, 11, 22, 23
X	JP, 52-63832, A (Taki Chemical Co., Ltd.), May 26, 1977 (26. 05. 77), Claim 1; page 2, lower left column, line 20 to page 3, upper right column, line 12 (Family: none)	1-9, 12-21, 24-30 10, 11, 22, 23
X	JP, 52-66839, A (Taki Chemical Co., Ltd.), May 26, 1977 (26. 05. 77), Claim 1; page 3, upper left column, line 15 to lower right column, line 12 (Family: none)	1-9, 12-21, 24-30 10, 11, 22, 23
Y	JP, 51-71588, A (Daido Chemical Industry Co., Ltd.), June 21, 1976 (21. 06. 76), Claim 1 (Family: none)	10, 11, 22, 23
Y	JP, 51-23448, A (K.K. chiyoda Kagaku Kenkyusho), February 25, 1976 (25. 02. 75), Claim 1; page 3, upper left column, lines 10 to 15 (Family: none)	10, 11, 22, 23
A	JP, 2-502655, A (The Commonwealth of Australia), August 23, 1990 (23. 08. 90), Claims 1 to 10 & EP, 347420, A & WO, 8806639, A	1 - 30
A	JP, 50-116338, A (Stouffer Chemical Co.), September 11, 1975 (11. 09. 75), Claim 1; page 2, upper right column, line 16 to lower right column, line 6 & US, 3969152, A & CA, 1014831, A	1 - 30
A	JP, 3-277790, A (Akuasu K.K.), December 9, 1991 (09. 12. 91), Claims 1, 3 (Family: none)	9-11, 21-23
A	JP, 4-300864, A (Mitsui Toatsu Chemicals, Inc.), October 23, 1992 (23. 10. 92), Claim 1 (Family: none)	9-11, 21-23
	JP, 50-93241, A (Nippon Kako Seishi Co., Ltd.), July 25, 1975 (25. 07. 75),	

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		PCT/JP97/00272
C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	Claim 1 (Family: none)	9-11, 21-23

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